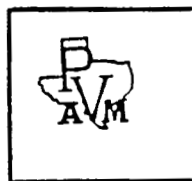


Preliminary Final Rpt.
9/6 - Final to Come

NGT-21-002-080
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UNIVERSITY ADVANCED SPACE DESIGN PROGRAM
PRAIRIE VIEW A&M UNIVERSITY

PHASE II-TASK 1-B
INTEGRATED WATER SYSTEM FOR A SPACE COLONY



**DESIGN OF A SURFACE—BASED FACTORY
FOR THE PRODUCTION
OF
LIFE—SUPPORT
AND
TECHNOLOGY—SUPPORT
PRODUCTS**

**PRAIRIE VIEW A&M UNIVERSITY
COLLEGE OF ENGINEERING
PRAIRIE VIEW, TEXAS**

JUNE, 1988

**(NASA-CR-184730) DESIGN OF A SURFACE-BASED
FACTORY FOR THE PRODUCTION OF LIFE SUPPORT
AND TECHNOLOGY SUPPORT PRODUCTS. PHASE 2:
INTEGRATED WATER SYSTEM FOR A SPACE COLONY
Preliminary Final (Prairie View Agricultural**

N89-19808

**Unclas
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14. COMMUNICATIONS AND CONTROL

NASA/USRA - ADVANCED DESIGN PROGRAM CONCEPTUAL
DESIGN OF AN INTEGRATED WATER SYSTEM FOR A
SPACE COLONY.

PROJECT ADVISOR: Dr. K. Fotouh, P.E.

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TASK

**DESIGN OF A SURFACE—BASED FACTORY
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PHASE I: SURVIVAL

TASK I: PRODUCTION AND PURIFICATION OF WATER
AND MANUFACTURING OF
BREATHABLE AIR

TASK II: PRODUCTION OF PROTEINS
AND FARMING

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PHASE II: SELF-SUFFICIENCY

TASK I: MFG. OF FUELS, CHEMICALS,
AGRICHEMICALS, PAINTS AND
PHARMACEUTICALS
(CARBON-BASED INDUSTRY)

TASK II: MFG. OF FERROUS AND NON-FERROUS
METALS AND ALLOYS, AND POLYMERIC
MATERIALS

TASK III: FABRICATION AND MACHINING OF
STRUCTURES, ENGINES, AND
EQUIPMENT

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**PHASE III:
PRODUCTION AND EXPORT TO
EARTH
(MATERIALS AND TECHNOLOGY)**

TASK I: REVIEW OF TECHNOLOGY

TASK II: MFG. OF ENZYMES AND HORMONES

TASK III: MFG. OF CRYSTALS

TASK IV: MFG. OF RADIATION RESISTANT MATERIALS

TASK V: OPEN FORUM

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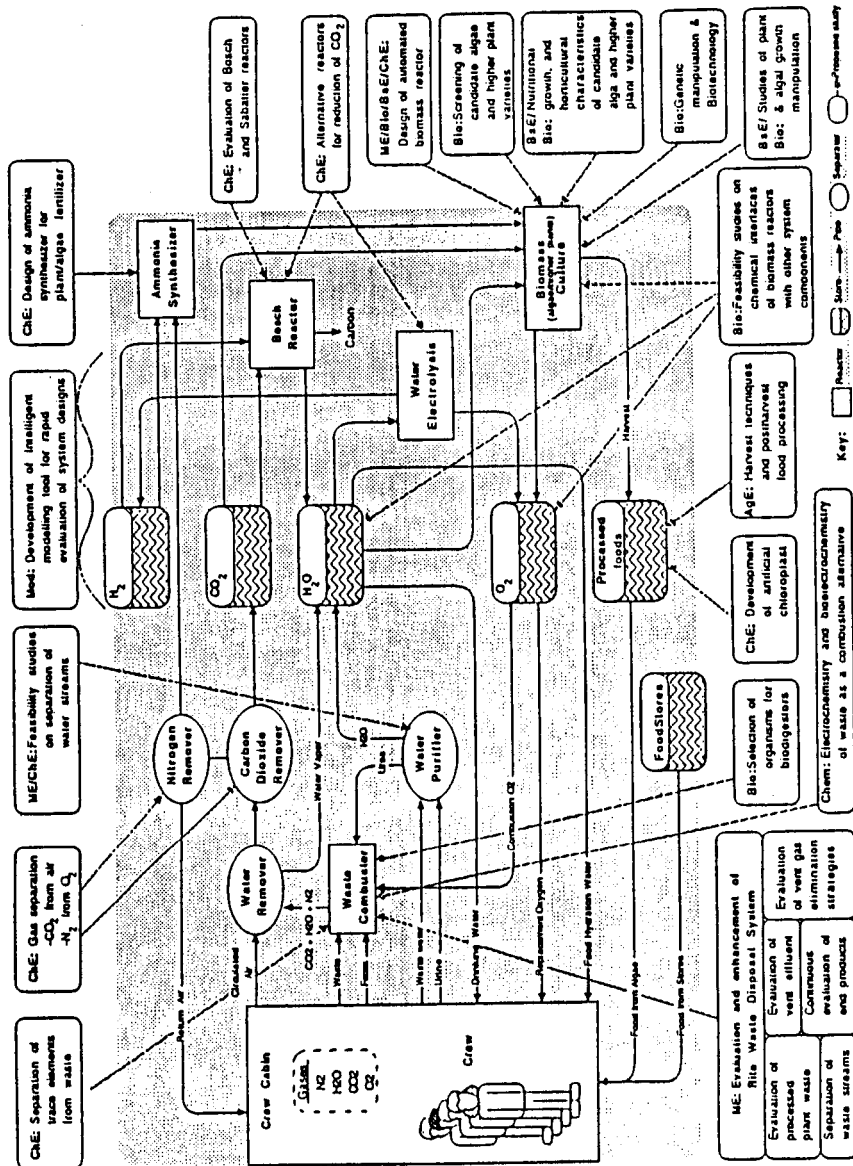
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NASA/USRA - ADVANCED DESIGN PROGRAM
PHASE II - TASK 1B

CONCEPTUAL DESIGN OF AN INTEGRATED WATER TREATMENT SYSTEM
TO SUPPORT A SPACE COLONY

SUMMARY:

In Phase II - Task 1A the Prairie View A&M University team completed the conceptual design of; a breathable air manufacturing system, a means of drilling for underground water, and storage of water for future use. The design objective of the team for the 1987-88 academic year (Phase II - Task 1B), has been the conceptual design of an integrated system for the supply of quality water for biological consumption, farming, residential and industrial use. The source of water for these applications is assumed to be artesian or subsurface.

The first step of the project was to establish the design criteria and major assumptions. Among these, we have included:

1. Water is scarce, therefore efficient water management through maximum recovery and reuse is critical.
2. Pollution problems will be minimized by exercising strict control on water discharge.
3. An effective hierarchial monitoring and control system will provide for quality control, and prompt attention to faulty equipment and leaks.
4. Since the pressure of the Martian atmosphere is only a small fraction of the earth atmosphere, all vessels and equipment must be sealed to prevent evaporation.
5. Three classes of water are defined: a. Water for farming must have a maximum mineral content such that plant life will flourish. b. Water for drinking must be free of pathogenic organisms and have a maximum salt content of less than 200 ppm. c. Water for manufacturing must be sufficiently free of ions such that they will not interfere with the manufacturing process or damage the quality of the product. d. Ion-free water will be provided for use in boilers in order to avoid erosion or corrosion of the materials of construction.

6. The various impurities which may be found in water and are reduced or removed at successive stages of treatment are:

turbidity, color, hardness, alkalinity, free mineral acid, carbon dioxide, pH, silica, oil, oxygen, hydrogen sulfide, ammonia, dissolved solids, suspended solids, organic solids, micro-organisms, and sulfate, chloride, nitrate, flouride, iron and manganese ions.

7. It has been assumed that the potential underground raw water supply resembles in quality from representative sources of underground water in Texas.

The assumed water impurities are:

	meq/l	ppm
Sodium Chloride {NaCl}	7.80	456.3
Magnesium Chloride {MgCl ₂ }	0.60	28.6
Magnesium Bi-Carbonate {Mg(HCO ₃) ₂ }	0.36	43.9
Calcium Bi-Carbonate {Ca(HCO ₃) ₂ }	0.57	46.2
Calcium Sulfate {CaSO ₄ }	3.07	208.0

8. Advanced technologies, which are not widely applied on earth, rather than traditional biological treatment, softening, and clarification techniques should be sought.

The second step of the effort was to generate a general block diagram of the expected treatment system and assign tasks to individual students. Among the treatment steps considered are:

sedimentation, softening, sand filtration, disinfection, ultrafiltration, reverse osmosis, demineralization, electrodialysis, vapor-compression evaporation, domestic waste treatment, and industrial waste handling.

At this early phase of study, no specific industries were selected, and hence no specific waste facilities were designed. It appears appropriate at this point in time to assume that evaporation by depressurization is a feasible means of recovering a major portion of the industrial waste water.

The list of processes for water purification and wastewater treatment given above suggests that there will be a need for on-site Chemicals manufacturing for ion-exchange regeneration, and disinfection.

The third step of the project was to set up a basis for the design capacity of the system. A total need of 10,000 gal/day was assumed required. It was also assumed that 30,000 raw-water intake volume is needed to produce the desired effluent volume. The following is a summary of the potential users and the level of treatment required:

APPLICATION	EFFLUENT
Farming	Municipal (domestic) wastewater treatment effluent. All waste produced by quarters and biological waste is directed to the waste water treatment facility. Additional water needed can be supplied by proper blending of reverse osmosis (stage 1) unit effluent and raw water to arrive to the desirable salinity level.
Domestic (Washing/Cooking)	The effluent from the reverse osmosis (stage 1) is disinfected and stored for use in the quarters.
Drinking	A part of the effluent from the reverse osmosis (stage 2) is disinfected and stored.
Processing (Manufacturing)	The major part of the reverse osmosis (stage 2) effluent is directed for this application.
Steam and Special Users	Ion-free deaerated water is produced for applications that require high purity water.

The fourth step of the project was for every individual student to screen the technology available and select the most suitable process(es) for his treatment phase. Detailed assumptions and criteria were established for each individual unit. As a result of these screening studies, the following sequence of treatment steps are selected for the system:

Sand Filtration: The purpose is to remove suspended solids with particle sizes of 10 microns and above. The process selected is a sand on gravel bed constructed on site. This has been chosen over cloth filtration and rotary vacuum filtration. The former is excluded because of the semi-manual nature of operation, the latter was excluded because of the moving parts and frequent need for maintenance. Figure 1 shows a guide for solid removal process selection.

Ultrafiltration: The process was selected as an additional cleaning step, for the removal of fine suspended solids; over microfiltration, centrifugation, and ultracentrifugation. Ultrafiltration was selected because it has a high removal efficiency for a wide range of particle sizes and has less moving parts. Size range of removal is 0.01 to 10 microns.

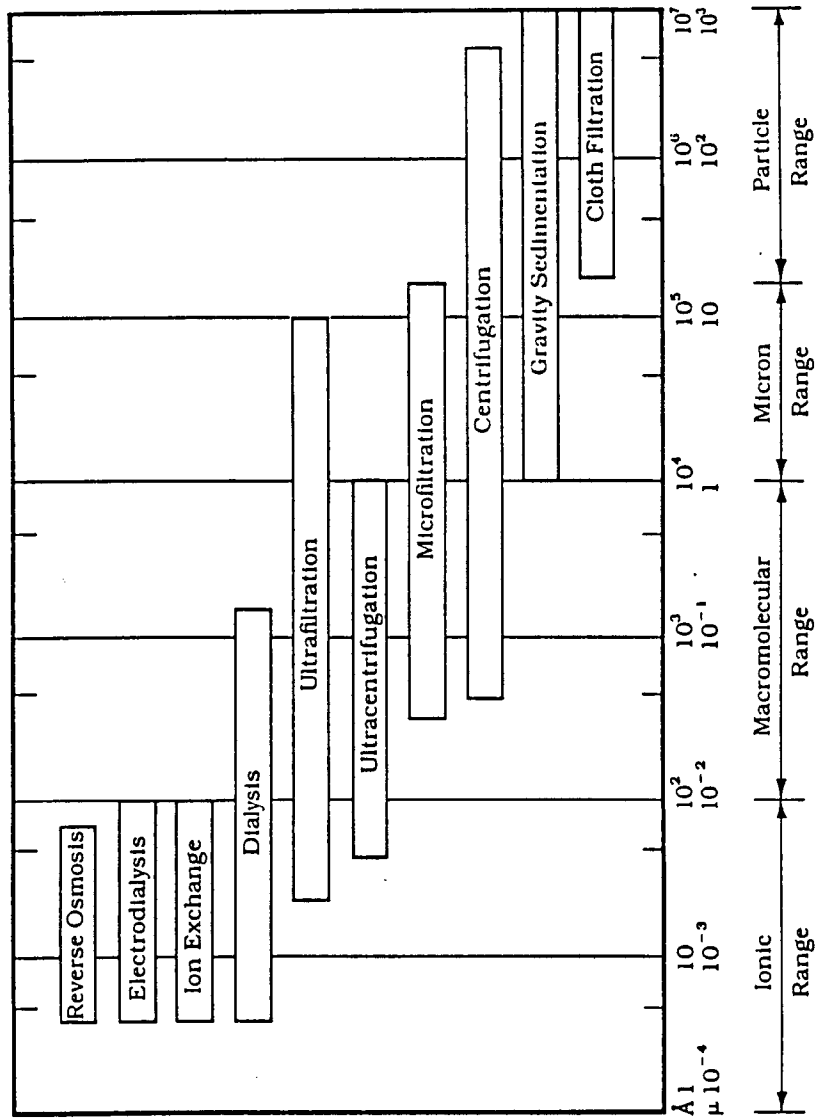
Reverse Osmosis: The process operation is based on increasing the pressure above the osmotic pressure of the brine solution to force clear water molecules across a permeable membrane. Two stages of reverse osmosis were preferred over one stage, each has a different membrane permeability. The first stage effluent can be used, in part, for domestic and farming applications. The remaining part of the first stage effluent is directed to the second stage osmosis process to produce extra clean water for industrial processing. The process was selected over electrodialysis for the lower power requirements, and over the ion exchange process for the size and weight.

Demineralization: This is an ion exchange process, and is being selected as a topping cleaning step to produce an ultra ion-free water for speciality manufacturing and steam making. The unit will be of much smaller size due to the fact that only a small part of the volumetric flowrate going through the second stage of the reverse osmosis unit will be demineralized.

Domestic Wastewater Treatment: The technology available is divided into two types based on cost only. The diversity of processes to select from is exemplified in Figure 2. Industrial wastewater facilities were not addressed at this point due to lack of information about the nature of contaminants produced.

A general arrangement of the designed system is shown in Figure 3. The industrial portion is hypothetically drawn and boxed for future analysis. The names of investigators are also written on the corresponding unit of the system.

Figure 1 Effective Ranges of Some Separation Techniques
 Adapted from "Membrane Separation Processes" by R. E. Lacey in Chemical Engineering, 4 September 1972.
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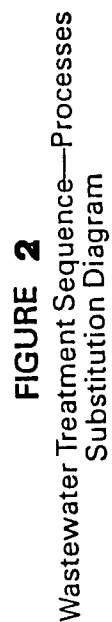


FIGURE 2

Wastewater Treatment Sequence—Processes Substitution Diagram

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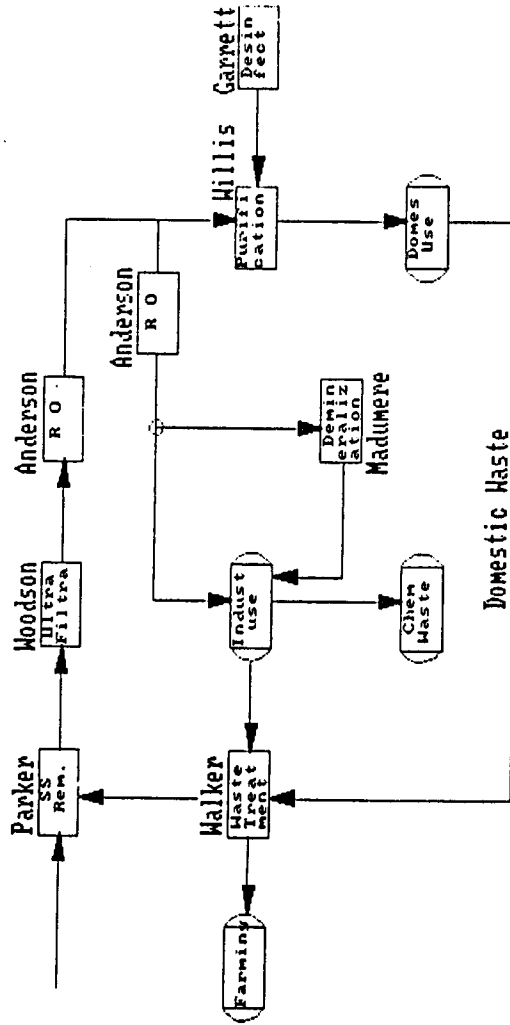
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SPACE COLONY PHASE II-TASK 1-B

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The diagram illustrates a complex water treatment and distribution system. The process begins with raw water intake, followed by pH control, suspended solids (S.S.) removal, ultra-filtration, and reverse osmosis (R.O.) Stage 1. The water then undergoes disinfection and is stored in tankage for treated water. A pump distributes this water to potable water storage and industrial use. Potable water storage feeds into a process unit, which has a reuse loop and a condensate return loop to boilers. Industrial use also feeds into the process unit. The process unit is connected to cooling towers, which provide makeup water and send water to process. The process unit also feeds into a boiler-feedwater treatment unit, which has a slowdown loop back to the process unit. The boiler-feedwater treatment unit feeds into a deaerator, which produces steam and has a slowdown loop back to the process unit. The deaerator also feeds into a facility water-treatment system. The facility water-treatment system has a reprocess loop back to the process unit and a slowdown loop back to the process unit. The facility water-treatment system also feeds into a spill/upset collection tank. The spill/upset collection tank has a flow diverter and a discharge line. The discharge line leads to a condenser, which then feeds into an evaporator. The evaporator has a solids disposal line. The condenser also feeds into a pump that leads to domestic use. Domestic use feeds into sanitary sewage, which then feeds into biological treatment. Biological treatment feeds into farming. Farming feeds into solids disposal. Solids disposal feeds into R.O. Stage 2, which then feeds into tankage for treated water.

FIGURE 3

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OBJECTIVE: PRODUCE 10 000 GALLONS OF TREATED WATER PER DAY FROM
AN INITIAL UNTREATED WATER SUPPLY EX THE DRILLING UNIT(S)
AT 30 000 GALLONS PER DAY

BREAKDOWN OF TREATED WATER

DEMINERALIZED	1 000 GAL/DAY
PERSONAL CONSUMPTION	1 000 GAL/DAY
MANUFACTURING	8 000 GAL/DAY



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ASSUMED WATER COMPOSITION ON MARS

	meq/l	ppm
NaCl	7.80	456.3
MgCl ₂	0.60	28.6
Mg(HCO ₃) ₂	0.36	43.9
Ca(HCO ₃) ₂	0.57	46.2
CaSO ₄	3.07	208.8



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CLASSIFICATION OF IMPURITIES


Suspended Solids	Organic
	Inorganic
Dissolved Solids	Organic
	Inorganic
Pathogenic Microorganisms	Aerobic
	Anaerobic




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APPLICATION	QUALITY LIMITATIONS (TDS) PPM	
Industrial	< 100	
Drinking	< 300	
Farming	< 2000	

<div data-bbox="557 1491 581 1719">APPLICATION</div> <div data-bbox="557 712 581 874">EFFLUENT</div> <div data-bbox="695 1576 719 1719">Farming</div> <div data-bbox="764 1189 789 1719">Domestic (washing/cooking)</div> <div data-bbox="834 1555 859 1719">Drinking</div> <div data-bbox="904 1253 928 1719">Process (manufacturing)</div> <div data-bbox="972 1270 997 1719">Steam and special uses</div> <div data-bbox="703 283 727 874">Domestic Wastewater Treatment</div> <div data-bbox="773 370 797 874">Reverse Osmosis (Stage 1)</div> <div data-bbox="842 370 867 874">Reverse Osmosis (Stage 2)</div> <div data-bbox="912 370 937 874">Reverse Osmosis (Stage 2)</div> <div data-bbox="980 534 1005 874">Ion Exchange Unit</div>	<div data-bbox="1292 1689 1386 1785">  </div> <div data-bbox="1292 721 1427 1498"> <p>NASA / USRA</p> <p>INTEGRATED WATER SYSTEM FOR A</p> <p>SPACE COLONY PHASE II-TASK 1-B</p> </div> <div data-bbox="1284 240 1443 614"> <p>DEPARTMENT OF CHEMICAL ENGINEERING</p> <p>ADVANCED DESIGN PROJECT</p> <p>APPROVED BY: K. FOTOUH</p> <p>PAGE:</p> </div>
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TREATMENT STEPS CONSIDERED

Sedimentation

Softening

Sand Filtration

Disinfection

Ultrafiltration

Reverse Osmosis

Deminerilization

Electrodialysis

Vapor-Compression Evaporation

Domestic Waste Treatment

Industrial Waste Treatment



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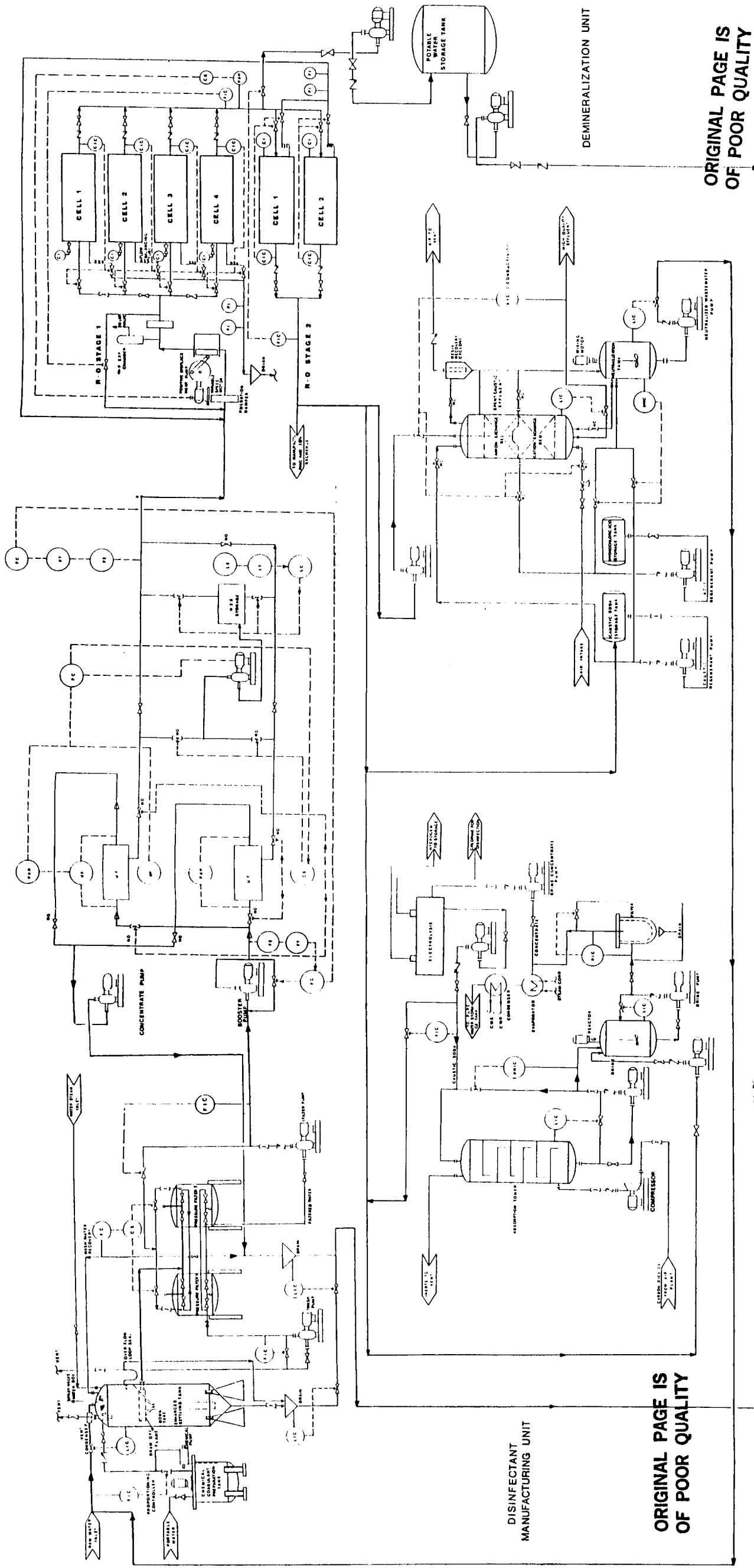
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SUSPENDED SOLIDS REMOVAL UNIT

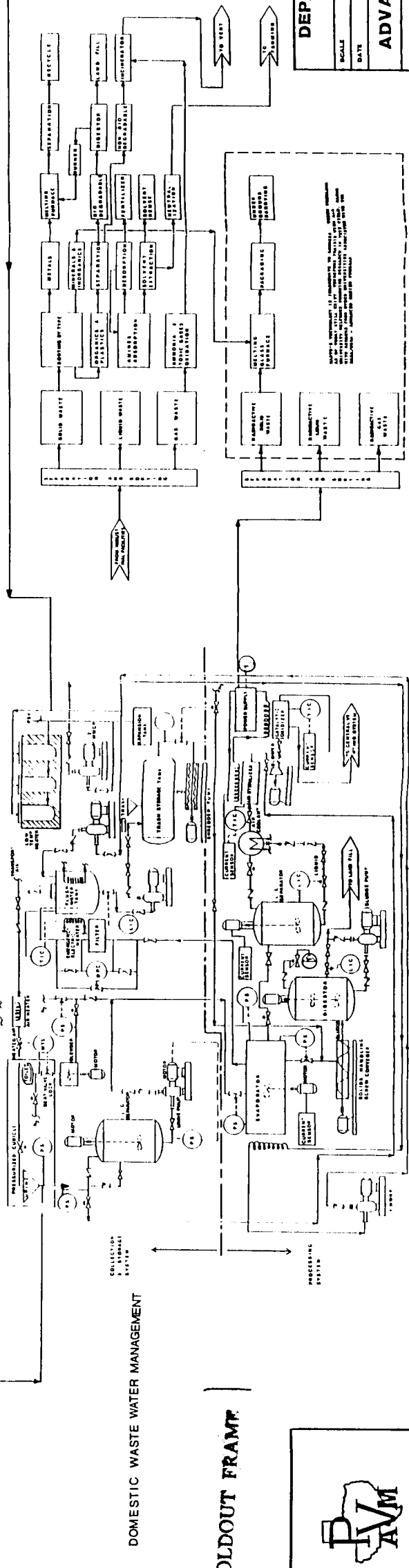
ULTRAFILTRATION UNIT

REVERSE OSMOSIS UNITS 1 & 2



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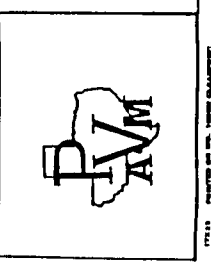
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PIPING SCHEDULE			
CODE DESIGNATION	SYSTEMS ¹	PIPE MATERIAL CLASSIFICATION	
		EXPOSED	BURIED, DUNDERED OR DULCIED
1	1M, 2M, 3M	2 INCHES	2 INCHES
2	4M	2 INCHES AND LARGER	2 INCHES AND LARGER
3	5M	2 INCHES AND LARGER	2 INCHES AND LARGER
4	6M	2 INCHES AND LARGER	2 INCHES AND LARGER
5	7M	2 INCHES AND LARGER	2 INCHES AND LARGER
6	8M	2 INCHES AND LARGER	2 INCHES AND LARGER
7	9M	2 INCHES AND LARGER	2 INCHES AND LARGER
8	10M	2 INCHES AND LARGER	2 INCHES AND LARGER
9	11M	2 INCHES AND LARGER	2 INCHES AND LARGER
10	12M	2 INCHES AND LARGER	2 INCHES AND LARGER
11	13M	2 INCHES AND LARGER	2 INCHES AND LARGER
12	14M	2 INCHES AND LARGER	2 INCHES AND LARGER
13	15M	2 INCHES AND LARGER	2 INCHES AND LARGER
14	16M	2 INCHES AND LARGER	2 INCHES AND LARGER
15	17M	2 INCHES AND LARGER	2 INCHES AND LARGER
16	18M	2 INCHES AND LARGER	2 INCHES AND LARGER
17	19M	2 INCHES AND LARGER	2 INCHES AND LARGER
18	20M	2 INCHES AND LARGER	2 INCHES AND LARGER
19	21M	2 INCHES AND LARGER	2 INCHES AND LARGER
20	22M	2 INCHES AND LARGER	2 INCHES AND LARGER
21	23M	2 INCHES AND LARGER	2 INCHES AND LARGER
22	24M	2 INCHES AND LARGER	2 INCHES AND LARGER
23	25M	2 INCHES AND LARGER	2 INCHES AND LARGER
24	26M	2 INCHES AND LARGER	2 INCHES AND LARGER
25	27M	2 INCHES AND LARGER	2 INCHES AND LARGER

- ¹PROTECTIVE WRAP ON BURIED LINES. A.S. ALUM. ALUM. AND GALV. TWO LAYERS OF FIBERGLASS REINFORCED CONCRETE. THIS REQUIREMENT DOES NOT APPLY TO LINES REQUIRING INSULATION.
- ²SYSTEM B-24 IS FOR PIPES LARGER THAN 4 INCHES IN DIAMETER. FOR SMALLER PIPES, USE SYSTEM B-2.
- ³FOR SITE STORM DRAINAGE PIPING, SEE SPECIFICATIONS FOR MATERIALS.
- ⁴MANUFACTURER SHALL CERTIFY THAT PIPE AND INSTALLATION IS ACCEPTABLE FOR OPERATING CONDITIONS AND PROVIDE GUARANTEE FOR BURIED PIPES OUTSIDE OF STRUCTURES. SEE SPECIFICATIONS FOR MATERIALS.
- ⁵CLASS LINE PIPE NOT REQUIRED FROM SLUDGE HEAT EXCHANGERS TO DIGESTERS.
- ⁶ENGINE INTAKE AND LUBRICATING OIL PIPING AND FITTINGS SHALL BE SCHEDULE 40 AND PICKLED AFTER FABRICATION IN ACCORDANCE WITH A.S. CE 1.1.
- ⁷CAST IRON PIPE SHALL NOT BE USED FOR EL, LO, LOR, LOS, TOL.
- ⁸CAST IRON PIPE MAY BE USED FOR 2" DRAIN LINES FROM EQUIPMENT PANS IN LIEU OF COPPER PIPE.
- ⁹LAP WELDED SLIP JOINTS AND EPDM LINING.
- ¹⁰SEE SPECIFICATIONS FOR INSULATION REQUIREMENTS.
- ¹¹PIPE AND FITTINGS CANNOT BE INSTALLED IN ACCORDANCE WITH MMS STD. SPEC. 94.1.19.
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PIPING SYSTEMS ABBREVIATIONS AND CODE DESIGNATION			
ABB	SYSTEM	CODE DESIGNATION	CODE DESIGNATION
AA	EXHAUST AIR	4	AS SPECIFIED
AB	CHILLED WATER RETURN	13	9
AC	CHILLED WATER SUPPLY	14	10
AD	CHILLED WATER RETURN	15	11
AE	CHILLED WATER SUPPLY	16	12
AF	CHILLED WATER RETURN	17	13
AG	CHILLED WATER SUPPLY	18	14
AH	CHILLED WATER RETURN	19	15
AI	CHILLED WATER SUPPLY	20	16
AJ	CHILLED WATER RETURN	21	17
AK	CHILLED WATER SUPPLY	22	18
AL	CHILLED WATER RETURN	23	19
AM	CHILLED WATER SUPPLY	24	20
AN	CHILLED WATER RETURN	25	21
AO	CHILLED WATER SUPPLY	26	22
AP	CHILLED WATER RETURN	27	23
AQ	CHILLED WATER SUPPLY	28	24
AR	CHILLED WATER RETURN	29	25
AS	CHILLED WATER SUPPLY	30	26
AT	CHILLED WATER RETURN	31	27
AU	CHILLED WATER SUPPLY	32	28
AV	CHILLED WATER RETURN	33	29
AW	CHILLED WATER SUPPLY	34	30
AX	CHILLED WATER RETURN	35	31
AY	CHILLED WATER SUPPLY	36	32
AZ	CHILLED WATER RETURN	37	33
BA	CHILLED WATER SUPPLY	38	34
BB	CHILLED WATER RETURN	39	35
BC	CHILLED WATER SUPPLY	40	36
BD	CHILLED WATER RETURN	41	37
BE	CHILLED WATER SUPPLY	42	38
BF	CHILLED WATER RETURN	43	39
BG	CHILLED WATER SUPPLY	44	40
BH	CHILLED WATER RETURN	45	41
BI	CHILLED WATER SUPPLY	46	42
BJ	CHILLED WATER RETURN	47	43
BK	CHILLED WATER SUPPLY	48	44
BL	CHILLED WATER RETURN	49	45
BM	CHILLED WATER SUPPLY	50	46
BN	CHILLED WATER RETURN	51	47
BO	CHILLED WATER SUPPLY	52	48
BP	CHILLED WATER RETURN	53	49
BQ	CHILLED WATER SUPPLY	54	50
BR	CHILLED WATER RETURN	55	51
BS	CHILLED WATER SUPPLY	56	52
BT	CHILLED WATER RETURN	57	53
BU	CHILLED WATER SUPPLY	58	54
BV	CHILLED WATER RETURN	59	55
BW	CHILLED WATER SUPPLY	60	56
BX	CHILLED WATER RETURN	61	57
BY	CHILLED WATER SUPPLY	62	58
BZ	CHILLED WATER RETURN	63	59
CA	CHILLED WATER SUPPLY	64	60
CB	CHILLED WATER RETURN	65	61
CC	CHILLED WATER SUPPLY	66	62
CD	CHILLED WATER RETURN	67	63
CE	CHILLED WATER SUPPLY	68	64
CF	CHILLED WATER RETURN	69	65
CG	CHILLED WATER SUPPLY	70	66
CH	CHILLED WATER RETURN	71	67
CI	CHILLED WATER SUPPLY	72	68
CJ	CHILLED WATER RETURN	73	69
CK	CHILLED WATER SUPPLY	74	70
CL	CHILLED WATER RETURN	75	71
CM	CHILLED WATER SUPPLY	76	72
CN	CHILLED WATER RETURN	77	73
CO	CHILLED WATER SUPPLY	78	74
CP	CHILLED WATER RETURN	79	75
CQ	CHILLED WATER SUPPLY	80	76
CR	CHILLED WATER RETURN	81	77
CS	CHILLED WATER SUPPLY	82	78
CT	CHILLED WATER RETURN	83	79
CU	CHILLED WATER SUPPLY	84	80
CV	CHILLED WATER RETURN	85	81
CW	CHILLED WATER SUPPLY	86	82
CX	CHILLED WATER RETURN	87	83
CY	CHILLED WATER SUPPLY	88	84
CZ	CHILLED WATER RETURN	89	85
DA	CHILLED WATER SUPPLY	90	86
DB	CHILLED WATER RETURN	91	87
DC	CHILLED WATER SUPPLY	92	88
DD	CHILLED WATER RETURN	93	89
DE	CHILLED WATER SUPPLY	94	90
DF	CHILLED WATER RETURN	95	91
DG	CHILLED WATER SUPPLY	96	92
DH	CHILLED WATER RETURN	97	93
DI	CHILLED WATER SUPPLY	98	94
DJ	CHILLED WATER RETURN	99	95
DK	CHILLED WATER SUPPLY	100	96
DL	CHILLED WATER RETURN	101	97
DM	CHILLED WATER SUPPLY	102	98
DN	CHILLED WATER RETURN	103	99
DO	CHILLED WATER SUPPLY	104	100
DP	CHILLED WATER RETURN	105	101
DQ	CHILLED WATER SUPPLY	106	102
DR	CHILLED WATER RETURN	107	103
DS	CHILLED WATER SUPPLY	108	104
DT	CHILLED WATER RETURN	109	105
DU	CHILLED WATER SUPPLY	110	106
DV	CHILLED WATER RETURN	111	107
DW	CHILLED WATER SUPPLY	112	108
DX	CHILLED WATER RETURN	113	109
DY	CHILLED WATER SUPPLY	114	110
DZ	CHILLED WATER RETURN	115	111
EA	CHILLED WATER SUPPLY	116	112
EB	CHILLED WATER RETURN	117	113
EC	CHILLED WATER SUPPLY	118	114
ED	CHILLED WATER RETURN	119	115
EE	CHILLED WATER SUPPLY	120	116
EF	CHILLED WATER RETURN	121	117
EG	CHILLED WATER SUPPLY	122	118
EH	CHILLED WATER RETURN	123	119
EI	CHILLED WATER SUPPLY	124	120
EJ	CHILLED WATER RETURN	125	121
EK	CHILLED WATER SUPPLY	126	122
EL	CHILLED WATER RETURN	127	123
EM	CHILLED WATER SUPPLY	128	124
EN	CHILLED WATER RETURN	129	125
EO	CHILLED WATER SUPPLY	130	126
EP	CHILLED WATER RETURN	131	127
EQ	CHILLED WATER SUPPLY	132	128
ER	CHILLED WATER RETURN	133	129
ES	CHILLED WATER SUPPLY	134	130
ET	CHILLED WATER RETURN	135	131
EU	CHILLED WATER SUPPLY	136	132
EV	CHILLED WATER RETURN	137	133
EW	CHILLED WATER SUPPLY	138	134
EX	CHILLED WATER RETURN	139	135
EY	CHILLED WATER SUPPLY	140	136
EZ	CHILLED WATER RETURN	141	137
FA	CHILLED WATER SUPPLY	142	138
FB	CHILLED WATER RETURN	143	139
FC	CHILLED WATER SUPPLY	144	140
FD	CHILLED WATER RETURN	145	141
FE	CHILLED WATER SUPPLY	146	142
FF	CHILLED WATER RETURN	147	143
FG	CHILLED WATER SUPPLY	148	144
FH	CHILLED WATER RETURN	149	145
FI	CHILLED WATER SUPPLY	150	146
FJ	CHILLED WATER RETURN	151	147
FK	CHILLED WATER SUPPLY	152	148
FL	CHILLED WATER RETURN	153	149
FM	CHILLED WATER SUPPLY	154	150
FN	CHILLED WATER RETURN	155	151
FO	CHILLED WATER SUPPLY	156	152
FP	CHILLED WATER RETURN	157	153
FQ	CHILLED WATER SUPPLY	158	154
FR	CHILLED WATER RETURN	159	155
FS	CHILLED WATER SUPPLY	160	156
FT	CHILLED WATER RETURN	161	157
FU	CHILLED WATER SUPPLY	162	158
FV	CHILLED WATER RETURN	163	159
FW	CHILLED WATER SUPPLY	164	160
FX	CHILLED WATER RETURN	165	161
FY	CHILLED WATER SUPPLY	166	162
FZ	CHILLED WATER RETURN	167	163
GA	CHILLED WATER SUPPLY	168	164
GB	CHILLED WATER RETURN	169	165
GC	CHILLED WATER SUPPLY	170	166
GD	CHILLED WATER RETURN	171	167
GE	CHILLED WATER SUPPLY	172	168
GF	CHILLED WATER RETURN	173	169
GG	CHILLED WATER SUPPLY	174	170
GH	CHILLED WATER RETURN	175	171
GI	CHILLED WATER SUPPLY	176	172
GO	CHILLED WATER RETURN	177	173
GP	CHILLED WATER SUPPLY	178	174
GQ	CHILLED WATER RETURN	179	175
GR	CHILLED WATER SUPPLY	180	176
GS	CHILLED WATER RETURN	181	177
GT	CHILLED WATER SUPPLY	182	178
GU	CHILLED WATER RETURN	183	179
GV	CHILLED WATER SUPPLY	184	180
GW	CHILLED WATER RETURN	185	181
GX	CHILLED WATER SUPPLY	186	182
GY	CHILLED WATER RETURN	187	183
GZ	CHILLED WATER SUPPLY	188	184
HA	CHILLED WATER RETURN	189	185
HB	CHILLED WATER SUPPLY	190	186
HC	CHILLED WATER RETURN	191	187
HD	CHILLED WATER SUPPLY	192	188
HE	CHILLED WATER RETURN	193	189
HF	CHILLED WATER SUPPLY	194	190
HG	CHILLED WATER RETURN	195	191
HH	CHILLED WATER SUPPLY	196	192
HI	CHILLED WATER RETURN	197	193
HJ	CHILLED WATER SUPPLY	198	194
HK	CHILLED WATER RETURN	199	195
HL	CHILLED WATER SUPPLY	200	196
HM	CHILLED WATER RETURN	201	197
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HO	CHILLED WATER SUPPLY	360	356
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HO	CHILLED WATER SUPPLY	362	358
HO	CHILLED WATER RETURN	363	359
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ORIGINAL PAGE IS
OF POOR QUALITY

NASA / USRA

INTEGRATED WATER SYSTEM FOR A SPACE COLONY PHASE II-TASK 1-B

DEPARTMENT OF CHEMICAL
ENGINEERING

ADVANCED DESIGN PROJECT

APPROVED BY: K. FOTOUH

PAGE

INSTRUMENT LEGEND			SYMBOLS FOR INSTRUMENTS			SYMBOLS FOR VALVES			ABBREVIATIONS			ABBREVIATIONS		
1ST LETTER AND SUCCEEDING LETTERS	OUTPUT FUNCTION	SYMBOL	DESCRIPTION	GRAPHIC SYMBOL	INSTRUMENT SYMBOL	SYMBOLS FOR VALVES	ABBREVIATIONS	ABBREVIATIONS	ACB	AL	ALT	AMP	AN	APP
A	ALARM		ALARM OPERATING		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	AL	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
B	BUZZER		BUZZER		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
C	CONDUCTIVITY		CONDUCTIVITY		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
D	DIFFERENTIAL		DIFFERENTIAL		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
E	ELONGATION		ELONGATION		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
F	FLOW		FLOW		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
G	TEMPERATURE		TEMPERATURE		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
H	HEIGHT		HEIGHT		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
I	LEVEL		LEVEL		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
J	MANUAL		MANUAL		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
K	TO LOW CONC.		TO LOW CONC.		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
L	PRESSURE		PRESSURE		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
M	QUANTITY		QUANTITY		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
N	CONCENTRATION		CONCENTRATION		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
O	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
P	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
Q	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
R	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
S	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
T	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
U	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
V	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
W	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
X	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
Y	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
Z	RECORD		RECORD		IV	ISOLATING VALVE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN

INSTRUMENT SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS			SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS			SYMBOLS FOR VALVES			ABBREVIATIONS			ABBREVIATIONS		
SYMBOL	DESCRIPTION	SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS	SYMBOLS FOR VALVES	ABBREVIATIONS	ABBREVIATIONS	SYMBOLS FOR VALVES	ABBREVIATIONS	ABBREVIATIONS	ACB	AL	ALT	AMP	AN	APP
	100 PSI INSTRUMENT AIR SUPPLY - FILTERED AND REGULATED	100 PSI INSTRUMENT AIR SUPPLY - FILTERED AND REGULATED	100 PSI AIR SUPPLY (GAS)	ACB	AIR CIRCUIT BREAKER	100 PSI AIR SUPPLY (GAS)	ACB	AIR CIRCUIT BREAKER	AL	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	100 PSI AIR SUPPLY (GAS)	100 PSI AIR SUPPLY (GAS)	PROCESS FLOW LINE	ACB	AIR CIRCUIT BREAKER	PROCESS FLOW LINE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	PROCESS FLOW LINE	PROCESS FLOW LINE	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	ACB	AIR CIRCUIT BREAKER	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	ACB	AIR CIRCUIT BREAKER	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	ACB	AIR CIRCUIT BREAKER	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	24V AC SUPPLY	ACB	AIR CIRCUIT BREAKER	24V AC SUPPLY	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	24V AC SUPPLY	24V AC SUPPLY		ACB	AIR CIRCUIT BREAKER		ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN

INSTRUMENT SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS			SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS			SYMBOLS FOR VALVES			ABBREVIATIONS			ABBREVIATIONS		
SYMBOL	DESCRIPTION	SYMBOLS FOR ELECTRICAL & PNEUMATIC SIGNALS	SYMBOLS FOR VALVES	ABBREVIATIONS	ABBREVIATIONS	SYMBOLS FOR VALVES	ABBREVIATIONS	ABBREVIATIONS	ACB	AL	ALT	AMP	AN	APP
	100 PSI INSTRUMENT AIR SUPPLY - FILTERED AND REGULATED	100 PSI INSTRUMENT AIR SUPPLY - FILTERED AND REGULATED	100 PSI AIR SUPPLY (GAS)	ACB	AIR CIRCUIT BREAKER	100 PSI AIR SUPPLY (GAS)	ACB	AIR CIRCUIT BREAKER	AL	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	100 PSI AIR SUPPLY (GAS)	100 PSI AIR SUPPLY (GAS)	PROCESS FLOW LINE	ACB	AIR CIRCUIT BREAKER	PROCESS FLOW LINE	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	PROCESS FLOW LINE	PROCESS FLOW LINE	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	ACB	AIR CIRCUIT BREAKER	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	TRANSMITTED PNEUMATIC SIGNAL (1-15 PSI/G)	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	ACB	AIR CIRCUIT BREAKER	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	TRANSMITTED DIRECT CURRENT SIGNAL (4-20 MA)	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	ACB	AIR CIRCUIT BREAKER	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	TRANSMITTED ELECTRICAL SIGNAL OTHER THAN 4-20MA	24V AC SUPPLY	ACB	AIR CIRCUIT BREAKER	24V AC SUPPLY	ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN
	24V AC SUPPLY	24V AC SUPPLY		ACB	AIR CIRCUIT BREAKER		ACB	AIR CIRCUIT BREAKER	ALT	ALTERNATE	ALTERNATING CURRENT	AMP	AMPERES	AN

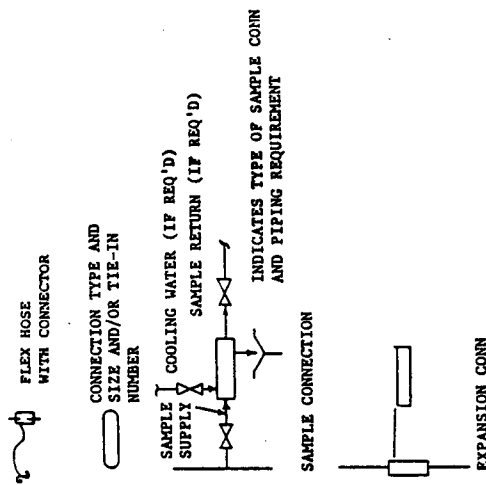
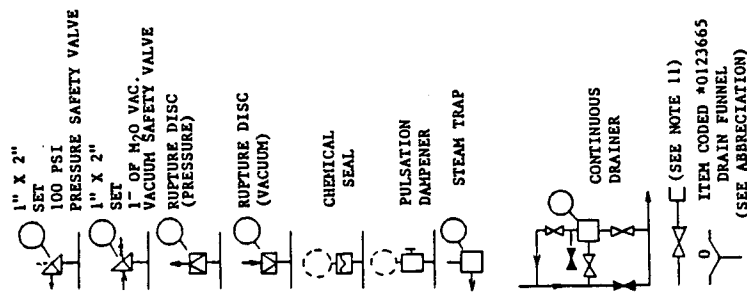
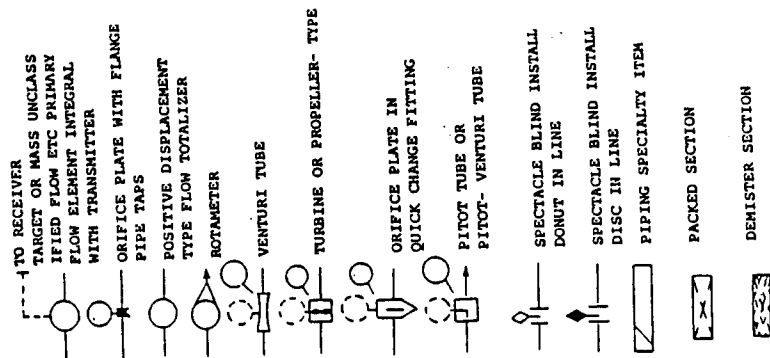
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MISCELLANEOUS



NASA/USRA INTEGRATED WATER SYSTEM FOR A SPACE COLONY PHASE II-TASK 1-B

DEPARTMENT OF CHEMICAL
ENGINEERING

NAME OF PROJECT
K. FOTOUH
ADVANCED DESIGN PROJECT

REVISION NUMBER

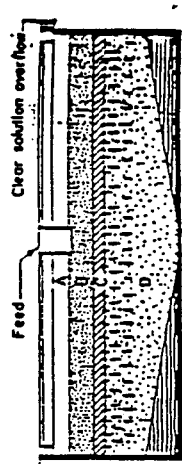
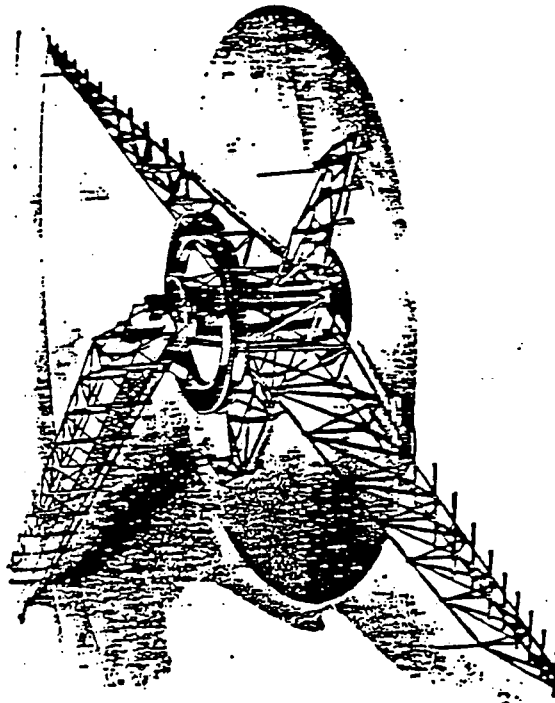
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MANUALLY OPERATED VALVES	CONTROL VALVES
<p>— GATE VALVE —</p> <p>— GLOBE VALVE —</p> <p>— CHECK VALVE —</p> <p>— PLUG VALVE —</p> <p>— HAND CONTROL VALVE —</p> <p>— BALL VALVE —</p> <p>— BUTTERFLY VALVE —</p> <p>— STOP CHECK VALVE —</p> <p>— BLOWDOWN VALVE —</p> <p>— OTHER VALVES —</p> <p>— INDICATE PROPER ABBREVIATION UNDER VALVE EXAMPLE —</p>	<p>— VALVE ACTION (SEE ABBREVIATION) —</p> <p>— ROTARY PLUG VALVE —</p> <p>— UNCLASSIFIED CONTROL VALVE —</p> <p>— MOTOR ACTUATED —</p> <p>— CONTROL VALVE WITH HAND ACTUATOR —</p> <p>— INDICATING ROTARY METER WITH AUTOMATIC THROTTLE VALVE —</p> <p>— CYLINDER ACTUATED VALVE —</p> <p>— REGULATOR SELF-CONTAINED —</p> <p>— REGULATOR WITH EXTERNAL PRESSURE TAP —</p> <p>— FLOW REGULATOR SELF-CONTAINED —</p> <p>— SOLENOID VALVE (WITH RESET) —</p> <p>— PRESSURE-BALANCED DIAPHRAGM ACTUATED —</p>

ABBREVIATIONS
<p>BD - BLOWDOWN</p> <p>CSC - CAR SEAL CLOSE</p> <p>CSO - CAR SEAL OPEN</p> <p>CW - COOLING WATER</p> <p>(F) - FURNISHED</p> <p>(F&P) - FURNISHED AND PIPED</p> <p>FC - FAIL CLOSE</p> <p>FI - FAIL INDETERMINATE</p> <p>FL - FAIL LOCKED</p> <p>FO - FAIL OPEN</p> <p>HP - HORSE POWER</p> <p>H.P.T - HIGH POINT</p> <p>IAS - INSTRUMENT AIR SUPPLY</p> <p>LC - LOCK CLOSE</p> <p>LO - LOCK OPEN</p> <p>LP - LOW PRESSURE</p> <p>L.P.T - LOW POINT</p> <p>ORB - ORBIT VALVE</p> <p>T/T - TANGENT TO TANGENT</p> <p>FP - FULL POINT</p> <p>FO - PUMP OUT</p> <p>SC - SAMPLE CONNECTION</p> <p>SO - STEAM OUT</p> <p>SP - SET POINT</p> <p>SP. GR. - SPECIFIC GRAVITY</p> <p>C - CHEMICAL DRAIN</p> <p>O - OILY WATER DRAIN</p> <p>S - STORM WATER DRAIN</p> <p>CO - CHAIN OPERATED</p> <p>GO - GEAR OPERATED</p> <p>OV - OPERATING VALVE</p> <p>TSO - TIGHT SHUT OFF</p> <p>FD - FLEX-DISC VALVE</p> <p>SS - SOFT SEAT VALVE</p> <p>TS - GENERAL TWIN-SEAL</p> <p>IC - INSULATION COLD</p> <p>Ih - INSULATION HOT</p> <p>Is - INSULATION SAFETY</p>

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	INTEGRATED WATER SYSTEM FOR A SPACE COLONY PHASE II-TASK 1-B		ADVANCED DESIGN PROJECT	
			DESIGNED BY	APPROVED BY
			K. FOTOUH	K. FOTOUH
			DATE	DATE
			ADVANCED DESIGN PROJECT	ADVANCED DESIGN PROJECT

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Section through a continuous thickener illustrating position of four zones of settling pulp

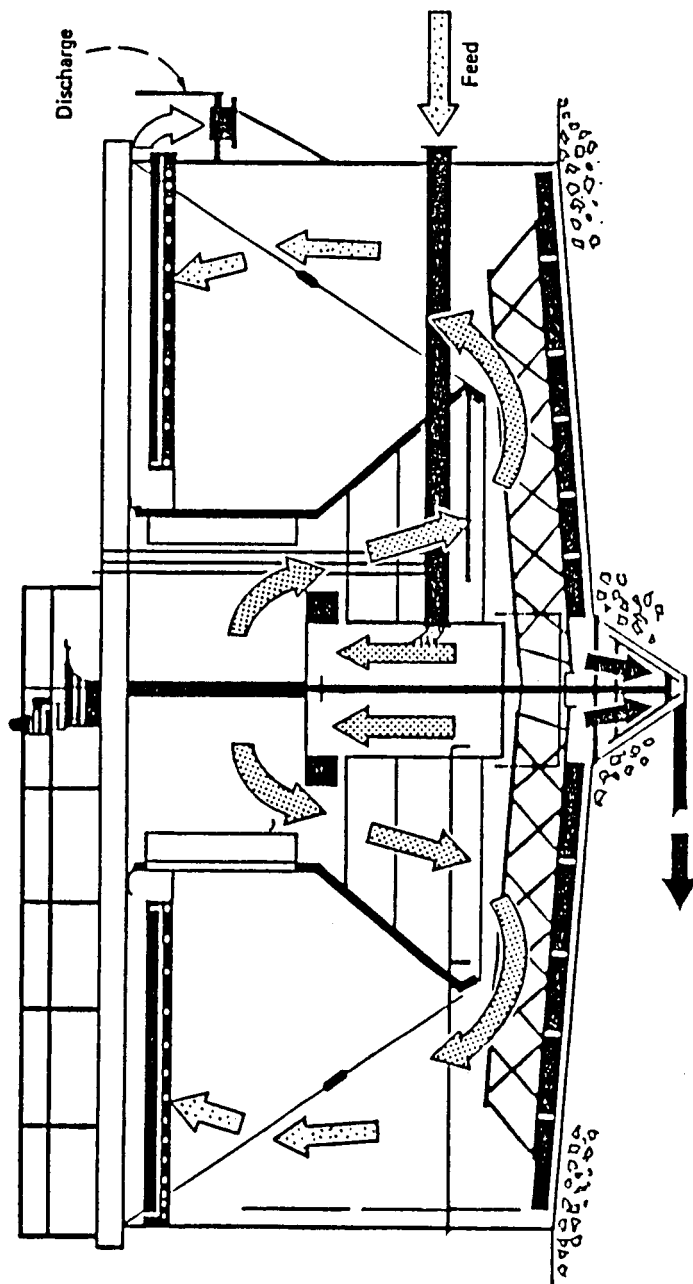
- ☐ Zone A: Clear water or solution
- ☒ Zone B: Pulp in transition from B to D consistency
- ☒ Zone C: Pulp in transition from C to D consistency
- ☒ Zone D: Pulp in compression consistency



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Solids-contact unit combines in a single basin mixing, coagulation and flocculation, liquid-solids separation and sludge removal



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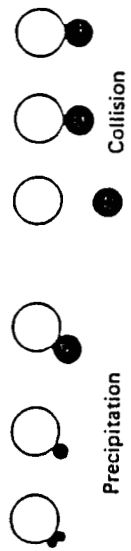
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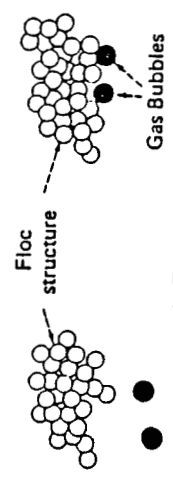
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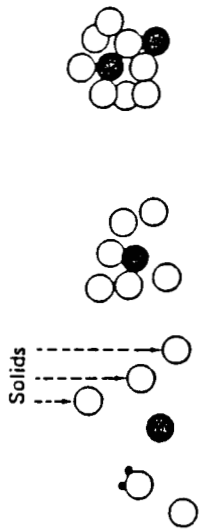
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a. Adhesion



b. Trapping



c. Adsorption

Mechanisms for attachment of gas bubbles
to solids or oil



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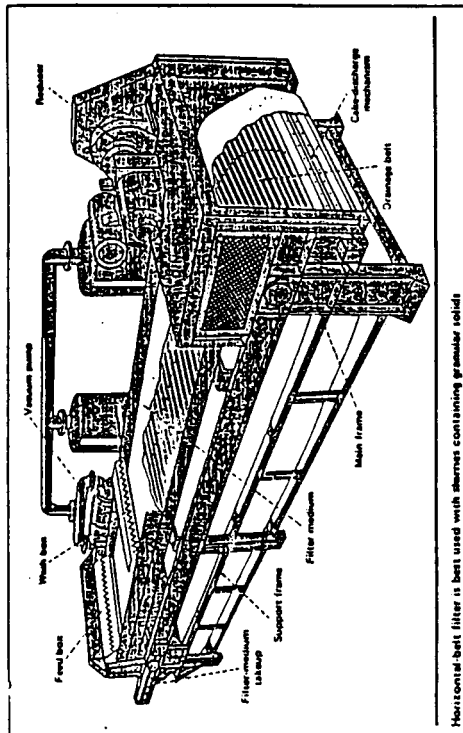
CONTINUOUS HORIZONTAL FILTERS

Advantages

- > Provide effective filtering of heavy, dense solids
- > Allow flooding of the cake with wash solvent
- > Easily adaptable to true countercurrent leaching or washing

Disadvantages

- > More expensive to build than drum filters
- > Use a relatively large amount of floor space per unit of filtering area



Horizontal-belt filter is best used with slurries containing granular solids



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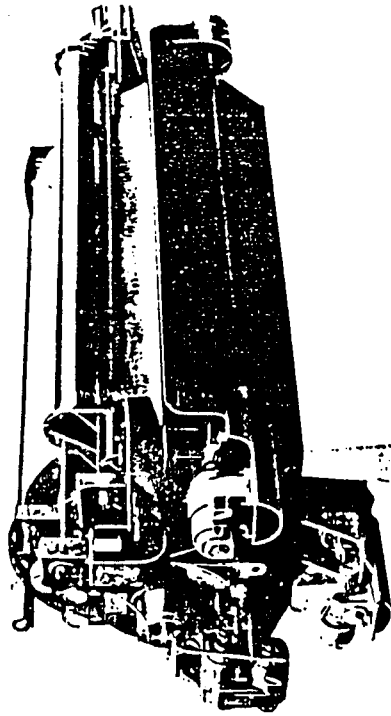
CONTINUOUS ROTARY DRUM FILTERS

Advantages

- > Usually designed as effective continuous filters
- > Low labor users and efficient adjuncts to continuous processes
- > Maintenance cost are usually low

Disadvantages

- > System must be maintained
- > Cannot be used with filtrates that are volatile
- > Most systems cannot handle difficulty filterable compressible solids



Continuous-vacuum precoat filter, 5 ft. 3 in. diameter x 8 ft face.
(Courtesy Dorr-Oliver, Inc.)



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Applications for granular-media gravity filters

Shallow-bed filters

(single medium, or multiple media)

1. Polishing clarified water.
2. Filtering flocculated low-turbidity waters.
3. Filtering sidestream from cooling towers.
4. Filtering waste solids.
5. Filtering tertiary effluents
6. Filtering after physical/chemical treatment.
7. Clarifying chemical processing streams
8. Recovering valuable suspended-solids products.

Deep-bed coarse-media filters

(single medium, or multiple media)

1. Clarifying steel-mill wastes.
2. Filtering tertiary effluents.



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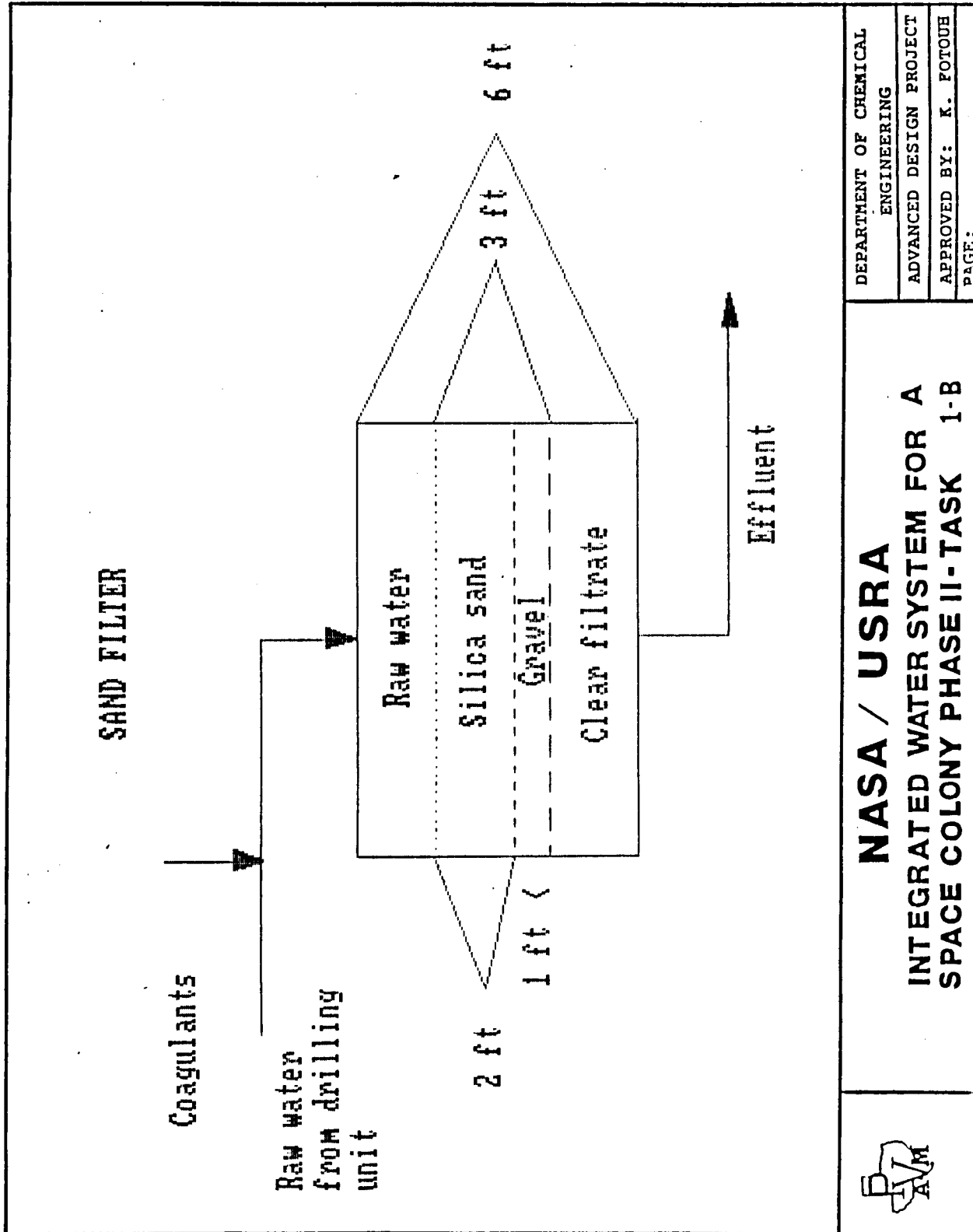
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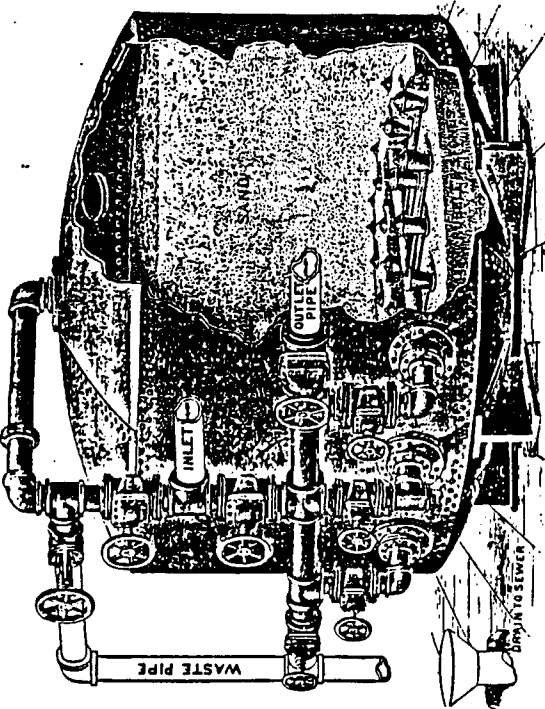
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SAND FILTERS



The Javelin Pressure Filter

Advantages

- > Very suitable for granular, or sandy crystalline solids
- > Low capital costs
- > Excellent equipment size range

Disadvantages

- > Severely limited when handling ease of cake discharge
- > Unacceptable for multiple-particle-size



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INTEGRATED WATER SYSTEM FOR A SPACE COLONY PHASE II-TASK 1-B

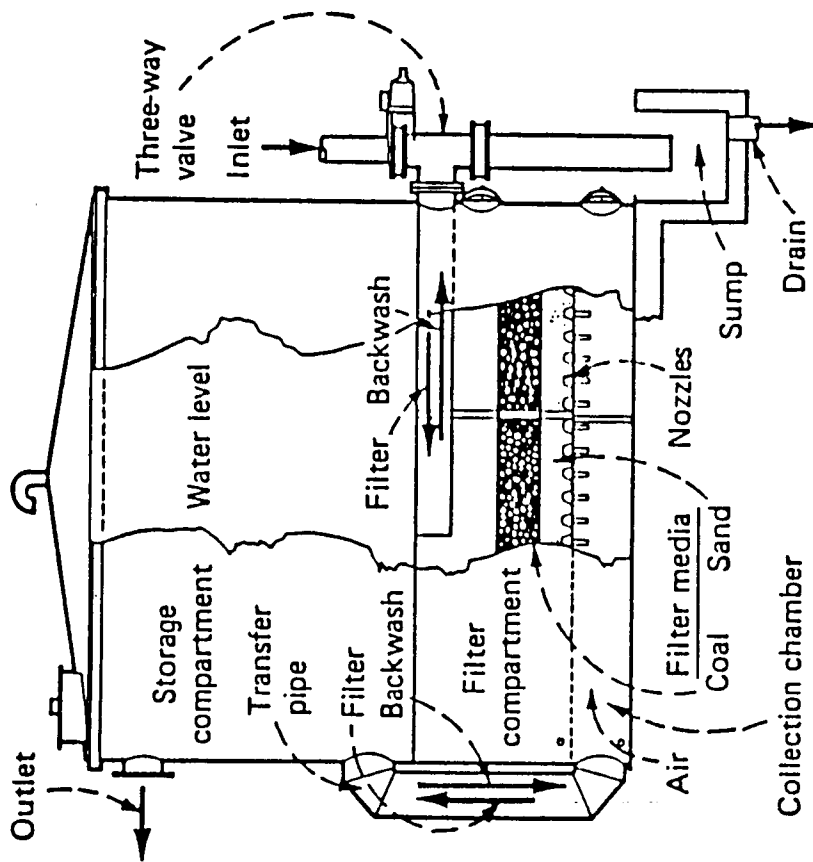
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Granular-media filter operates on
a controlled cycle



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DECISION CHART

EQPT	CONTINUOUS OPERATION	EQUIPMENT SIZE	OPTIMUM PARTICLE SIZE	POWER CONSUMPTION	MAINTENANCE	OPTIMUM CONCENTRATION	TOTAL
HORIZONTAL FILTERS	8	5	7	6	8	8	730
ROTARY DRUM FILTERS	8	7	8	5	6	9	740
SAND FILTERS	6	7	8	8	9	8	770
SCREENS	7	9	9	7	7	7	760
	(20)	(10)	(20)	(10)	(20)	(20)	



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DESIGN ASSUMPTIONS

Flowrate 10,000 gallons/day

Gravity = 3/8 earths gravity

Stokes law applies to settling

Return sludge concentration is 7000 mg/L

Temperature 20° C



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DESIGN RECOMMENDATIONS

Primary Clarifier

SETTLING VELOCITIES	12 - 18 m ³ /m ² day
SURFACE AREA	2.7 m ²
DEPTH OF TANK	1.0 m
TOTAL VOLUME	2.7 m ³
DETENTION TIME	2 hours

Biological Reactor

REACTOR VOLUME	1.5 m ³
AERATION TIME	60 min (approx.)
OXYGEN REQUIREMENT	7.0 kg/day
TREATMENT EFFICIENCY	97%

Secondary Clarifier

SURFACE AREA	4.7 m ²
DEPTH OF TANK	1.5 m
TOTAL VOLUME	7.1 m ³



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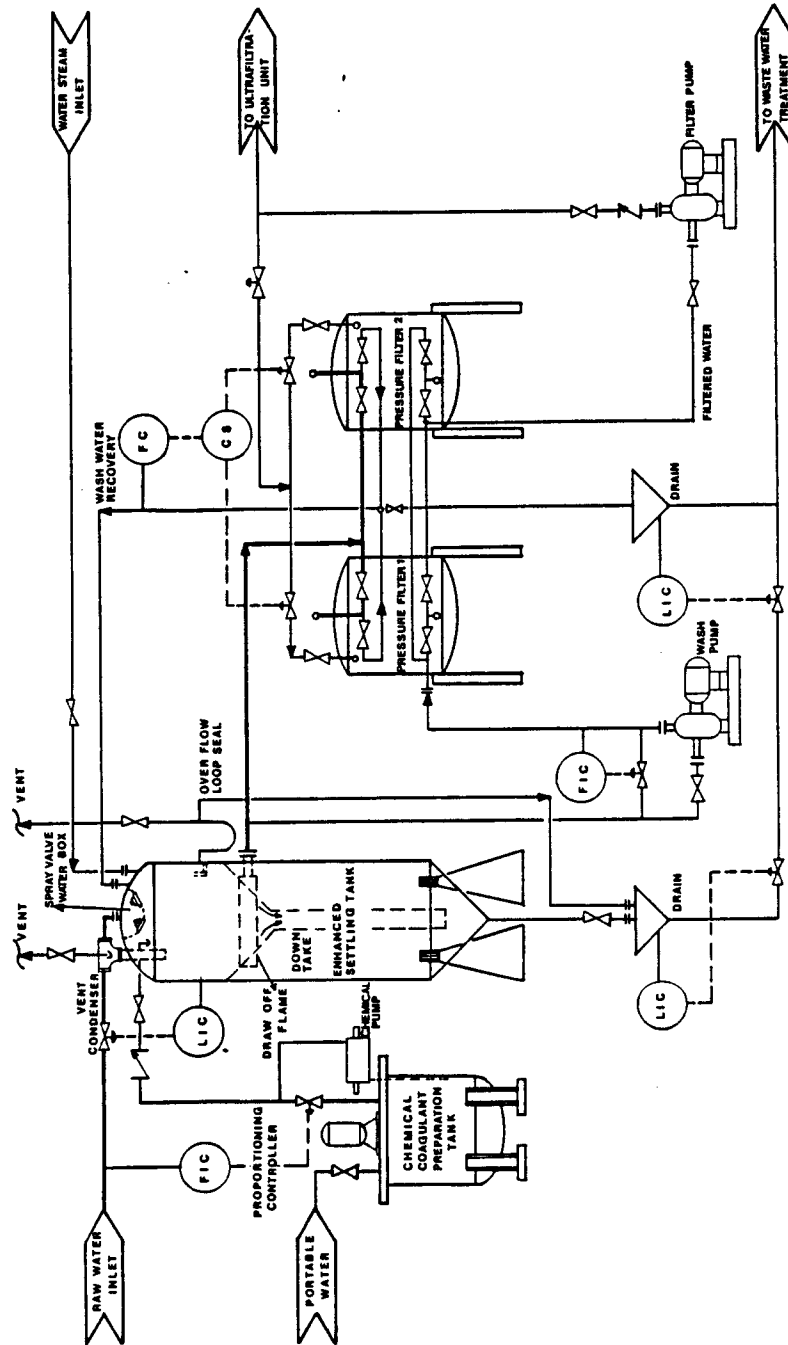
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2 SUSPENDED SOLIDS REMOVAL UNIT



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Technique	Applications	Limitations	Relative costs		Comments
			Capital	Operating	
Vapor-compression evaporation	Concentration of wastewater or cooling-tower blowdown Concurrent production of high-purity water	Not for organics that form azeotropes or steam-distill Fouling must be controllable	High	High	Rapid growth High-quality distillate Handles broad range of contaminants in water
Waste heat evaporation	Concentration of wastewater	Not for organics that form azeotropes or steam-distill	Medium	Medium	Not widely used now Future potential good
Reverse osmosis, ultrafiltration	Condensate recovery Removal of ionized salts, plus many organics Recovery of heavy metals, colloidal material Production of ultrapure water	Fouling-sensitive Stream must not degrade membranes Reject stream may be high-volume	Medium	Medium	Future potential strong Intense application development underway
Electrodialysis	Potable water from saline or brackish source	Limited to ionizable salts	Medium-high	Medium	Modest future potential
Steam stripping	Recovery of process condensates and other contaminated waters Removal of H_2S , NH_3 , plus some light organics	Stripped condensates may need further processing	Medium	Medium-high	Well-established as part of some processes
Combination wet/dry cooling towers	Puts part of tower load on air fins Can cut fogging	Costly compared with wet cooling tower	Medium	Medium	Growth expected in arid areas
Air-fin cooling	Numerous process applications	For higher-level heat transfer Can be prone to freeze-up, waxing	Medium	Medium	Well-established Good for higher-temperature heat rejection
Sidestream softening	Reduce cooling-tower blowdown	Dissolved solids must be removable Control can be difficult	Low-medium	Low-medium	Not widely used Future potential good



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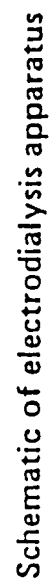
Technique	Applications	Limitations	Relative costs		Comments
			Capital	Operating	
Vapor-compression evaporation	Concentration of wastewater or cooling-tower blowdown Concurrent production of high-purity water	Not for organics that form azeotropes or steam-distill Fouling must be controllable	High	High	Rapid growth High-quality distillate Handles broad range of contaminants in water
Waste heat evaporation	Concentration of wastewater Condensate recovery	Not for organics that form azeotropes or steam-distill	Medium	Medium	Not widely used now Future potential good
Reverse osmosis, ultrafiltration	Removal of ionized salts, plus many organics Recovery of heavy metals, colloidal material Production of ultrapure water Potable water from saline or brackish source	Fouling-sensitive Stream must not degrade membranes Reject stream may be high-volume	Medium	Medium	Future potential strong Intense application development underway
Electrodialysis	Recovery of process condensates and other contaminated waters Removal of H_2S , NH_3 , plus some light organics	Limited to ionizable salts	Medium-high	Medium	Modest future potential
Steam stripping	Recovery of process condensates and other contaminated waters Removal of H_2S , NH_3 , plus some light organics	Stripped condensates may need further processing	Medium	Medium-high	Well-established as part of some processes
Combination wet/dry cooling towers	Puts part of tower load on air fins Can cut fogging Numerous process applications	Costly compared with wet cooling tower	Medium	Medium	Growth expected in arid areas
Air-fin cooling	Reduce cooling-tower blowdown	For higher-level heat transfer Can be prone to freeze-up, waxing Dissolved solids must be removable Control can be difficult	Medium	Medium	Well-established Good for higher-temperature heat rejection
Sidestream softening			Low-medium	Low-medium	Not widely used Future potential good



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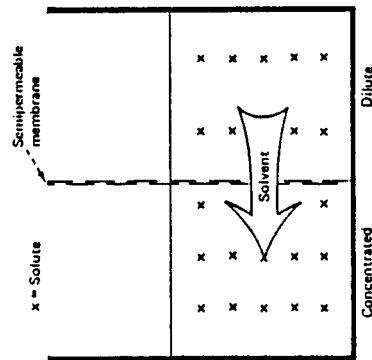
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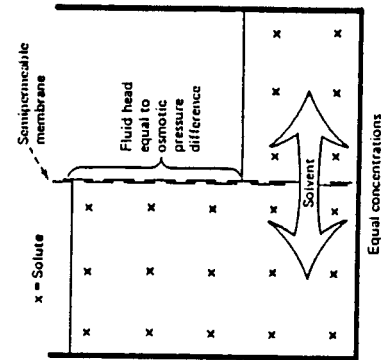
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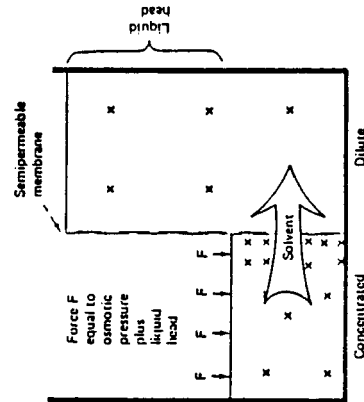
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DIRECT OSMOSIS: solvent flows spontaneously through semipermeable membrane



SOLVENT FLOW stops when the osmotic pressures of two solutions are equal



REVERSE OSMOSIS requires applied force equal to osmotic pressure plus liquid head



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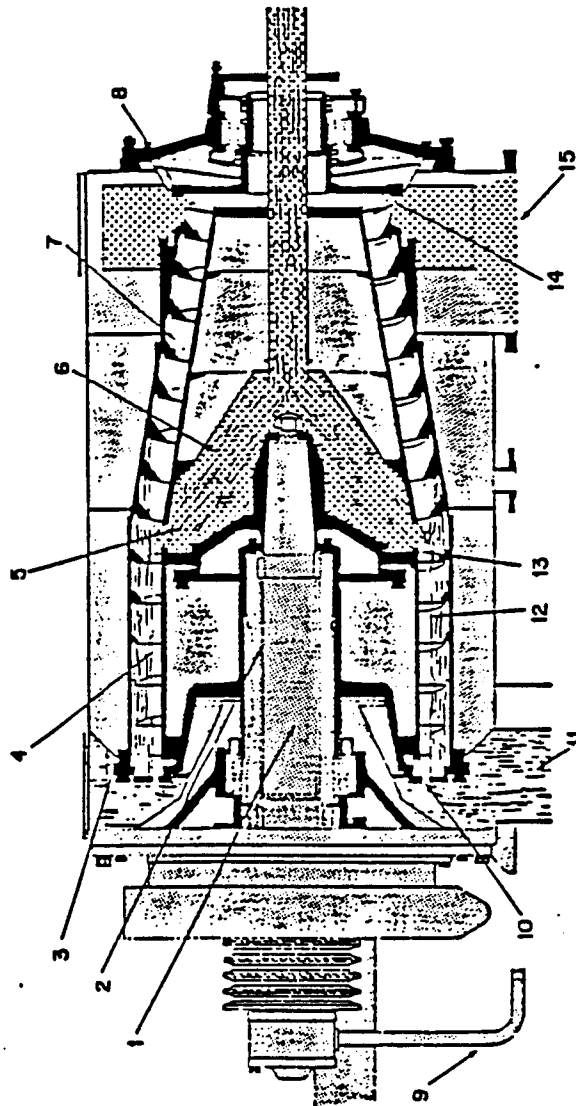
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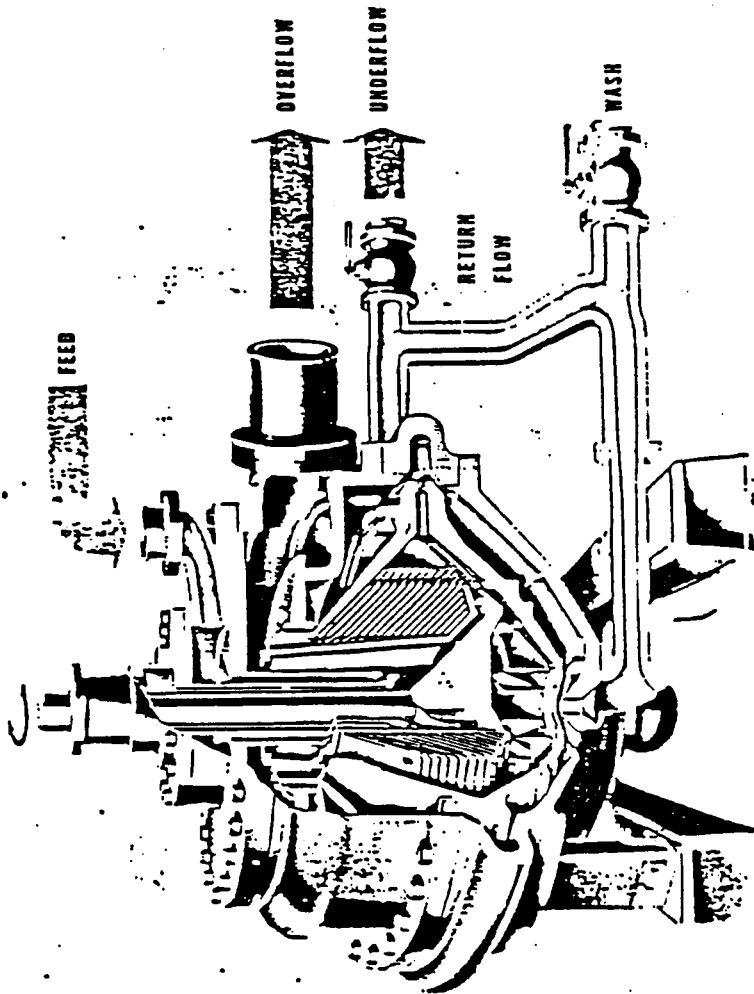
Continuous horizontal or vertical vibratory centrifuge. (1) Conveyor output eccentric shaft, (2) bowl output shaft, (3) effluent bowl head, (4) conveyor, (5) bowl, (6) feed compartment, (7) bench, (8) cake pump, (9) torque arm, (10) pool settling, (11) effluent, (12) pool volume, (13) feed ports, (14) cake ports, (15) cake solids. (Emswile Corp.)



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Peripheral-discharge-disk centrifuge. (Dorr-Oliver Incorporated.)



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TECHNOLOGY RATINGS
Table-II

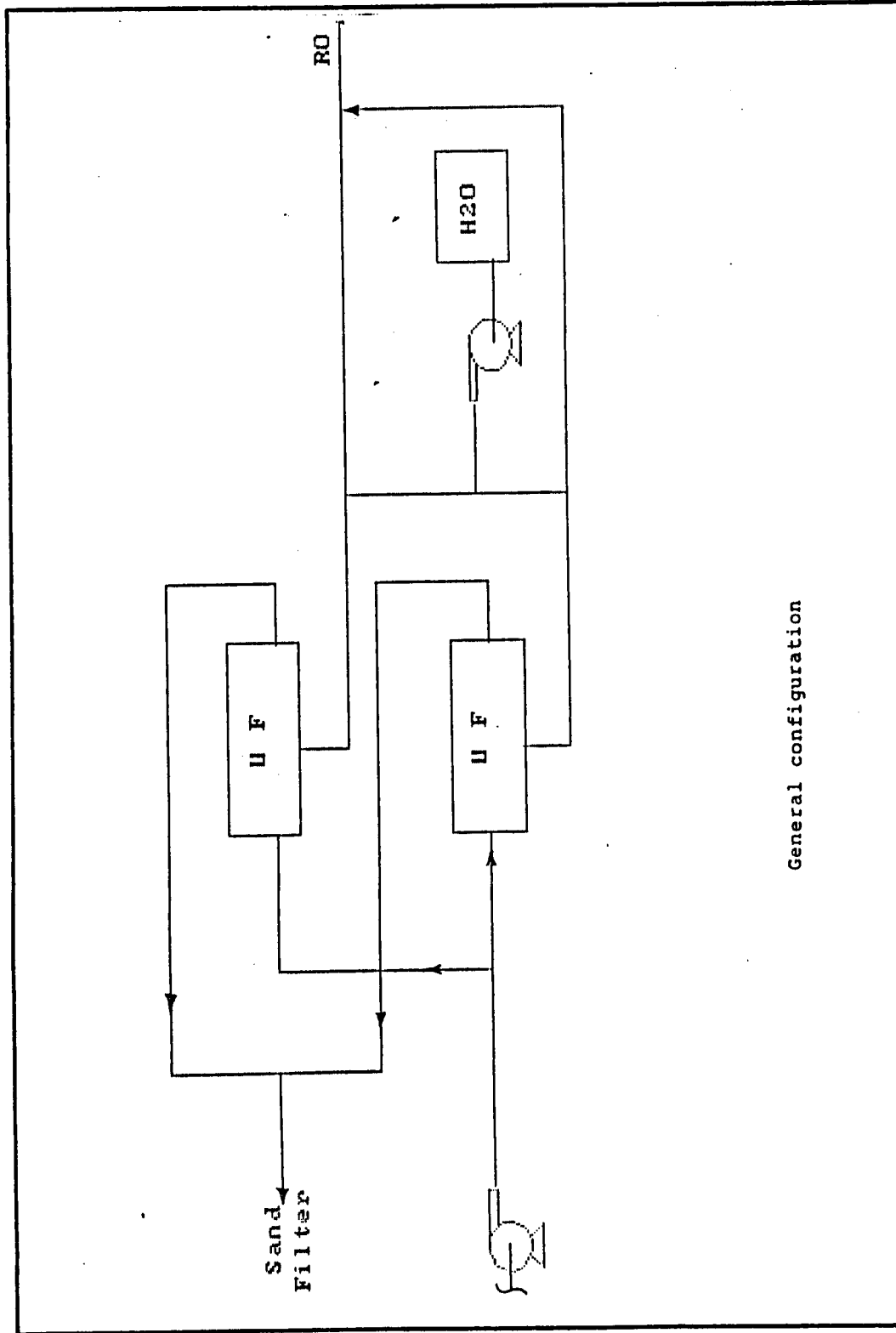
Type	Operating Temp	Particle Size Retention Range	Continuous Operation	Relative Equipment Weight	Maintainability	Total
*1	10	6	5	3	5	29
2	10	5	5	3	5	28
3	10	10	8	5	2	35
4	10	7	7	8	7	39
5	10	10	9	8	8	45

1:Continuous horizontal, conveyer type solid bowl centrifuge.
 2:Peripheral-discharge-disk centrifuge.
 3:Chemical coagulation & clarifiers.
 4:Microfiltration.
 5:Ultrafiltration.



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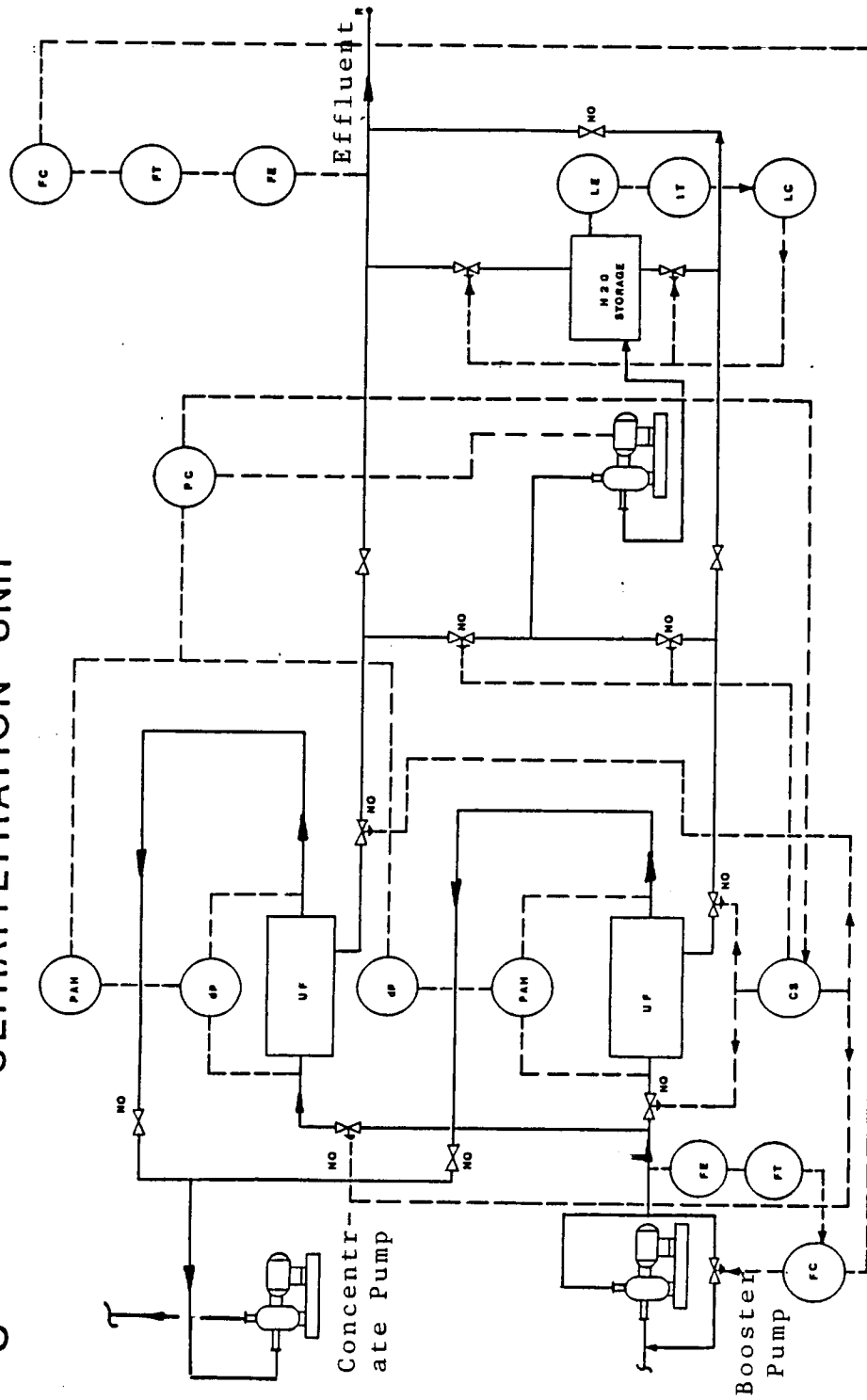


General configuration

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ULTRAFILTRATION UNIT



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Membrane Cleaning Techniques for Hyperfiltration

Technique	Method	Description
Physical	Mechanical	Foam ball swabbing
	Hydrodynamical	Tangential velocity variation
	Backwashing	Turbulence promoters
	Air-Water flushing Sonication	Depressure and forced or osmotic reverse flow of product Daily 15 min depressurized flush Regular ultrasonic cleaning with wetting agent
Chemical	Reverse flow Additives to feed	Reverse flow direction of feed pH control to reduce hydrolysis and scale deposit 5 ml/gal of 5% sodium hypochlorite at pH 5 Friction reducing additives (polyethylene glycol) soil dispersants (sodium silicate) Complexing agents (EDTA, Sodium hexametaphosphate) Oxidizing agents (citric acid)
	Flushing with additives at low pressure	Detergents (1% BIZ)
Other	Membrane replacement Inorganic membranes Active insoluble enzymes attached to membrane	High concentration of NaCl (18%) in situ membrane replacement Encourage biogrowth to consume fouling film Degradation of fouling film
	Polyelectrolyte membranes Precoat protection	Composite membranes or dynamic layer technique Precoat (diatomaceous earth, activated carbon, and surface-active agent) Deposit a porous diatomaceous earth coating



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Membrane Number	Salt Rejection (%) [*]	Flux m ³ /m ² /d (gfd) ^{**}	Test Conditions
NTR-1597	97	0.7(17)	0.5% NaCl solution 42 Kg/cm ² (600 psig) 25° C (77° F)
NTR-1595	95	0.8(20)	
NTR-1590	90	1.2(30)	
NTR-1570	70	0.8(20)	0.5% NaCl solution 20 Kg/cm ² (285 psig) 25° C (77° F)
NTR-1550	50	1.3(32)	
NTR-1530	30	1.5(37)	
NTR-1510	10	2.5(62)	

^{*} nominal

^{**} gallons per square foot per day

Typical rejection of organics by NTR-1597 membrane

Species	Rel. (%)
Sucrose	100
Lactose	100
Glucose	99.9
Protein	100
Water-soluble starch	100
Dyes	100
Bacteria and Virus	100
Nonionic surfactant	95~99
Anionic surfactant	90~95
Phenol	negative*
Acetic acid	**
Lactic acid	**
Alcohol	0~80***
BOD	85~99
COD	85~99

*Permeate is actually enriched due to preferential passage through the membrane.

**Dependent on pH

***Dependent on the form of alcohol

Typical rejections of inorganic ions by NTR-1597 membrane

IONS	Rel. (%)
Na ⁺	95 ~ 97
K ⁺	94 ~ 97
Ca ²⁺	96 ~ 99
Mg ²⁺	96 ~ 99
Cu ²⁺	96 ~ 99
Ni ²⁺	97 ~ 99
Sn ²⁺	98 ~ 99
Cd ²⁺	98 ~ 99
Al ³⁺	99
Fe ³⁺	99
Cl ⁻	95 ~ 97
F ⁻	95 ~ 97
NO ₃ ⁻	93 ~ 96
CN ⁻	90 ~ 95
SO ₄ ²⁻	99
PO ₄ ³⁻	99

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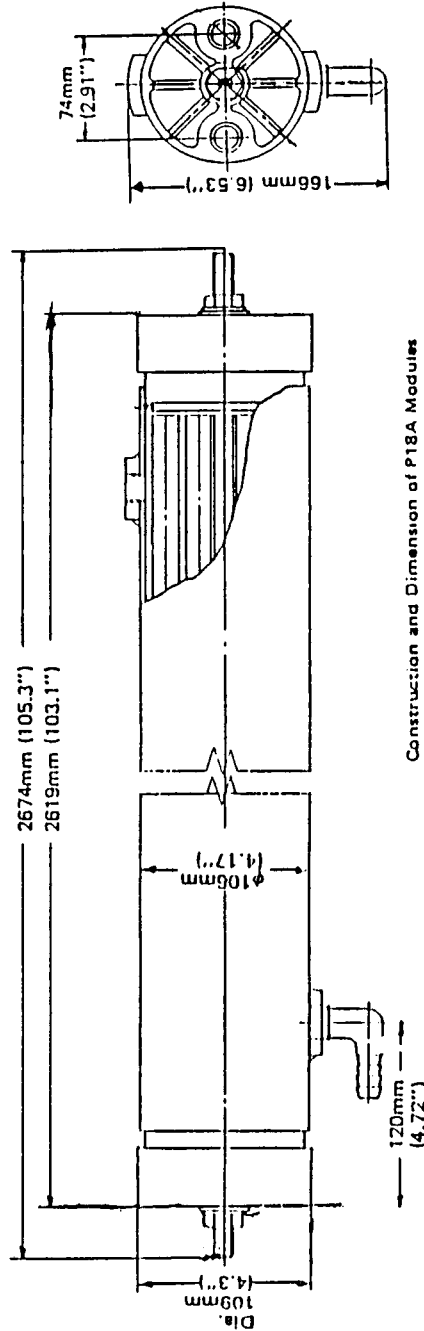
Module Specifications

Number of Tubes	18
Membrane Area	1.62m ² (17.4 sq. ft.)
Diameter	109mm (4.3")
Length	2619mm (103")

NTR-1597 SERIES P18-A TUBULAR MODULE

NITTO DENKO AMERICA, INC.

1. Feed Concentrate Header
2. Air Vent
3. FPR Tube (18)
4. Return Header
5. Permeate Nozzle



Construction and Dimension of P18A Modules



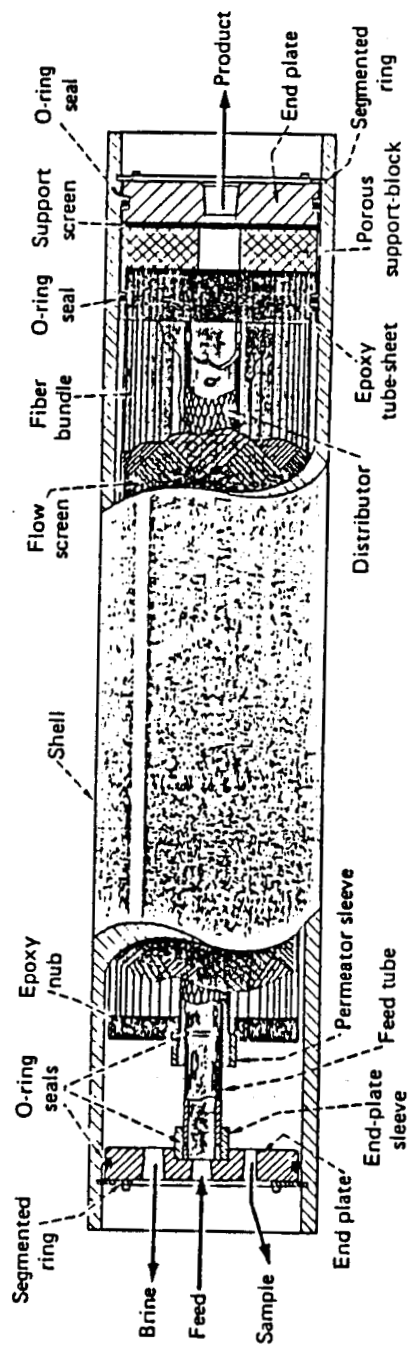
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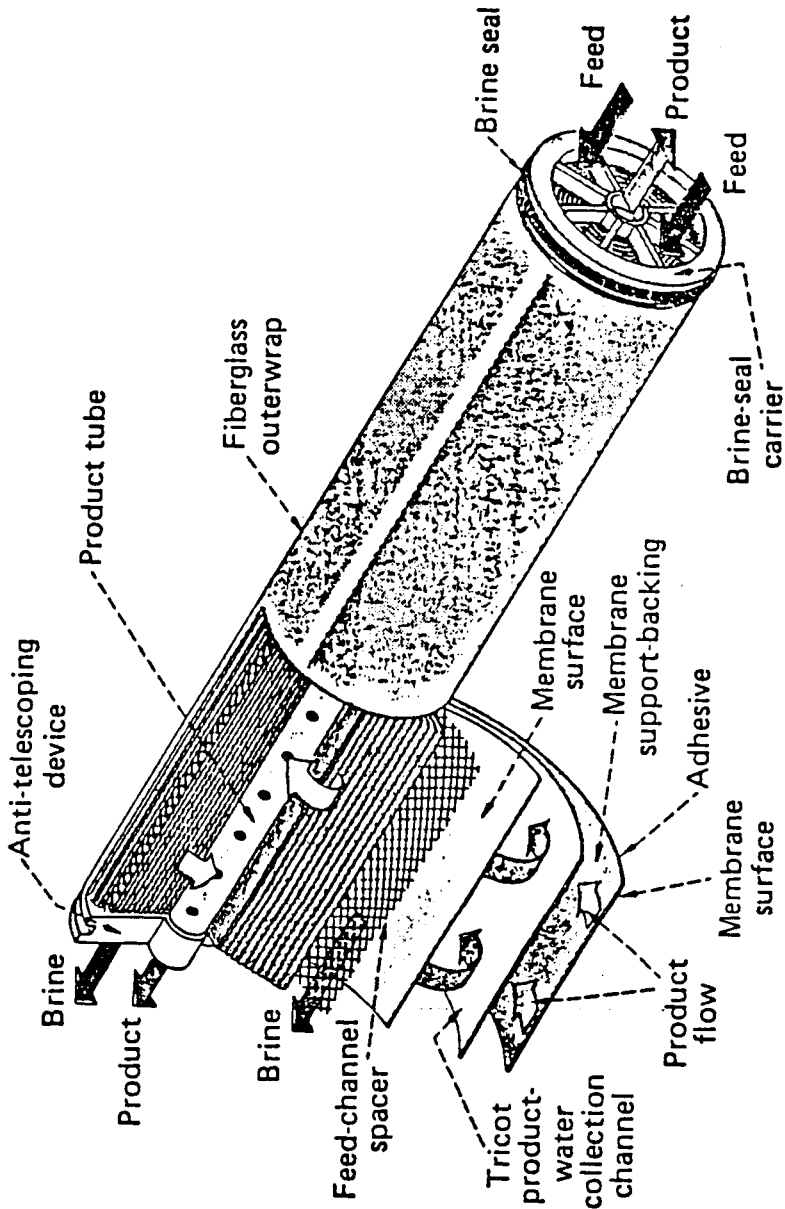
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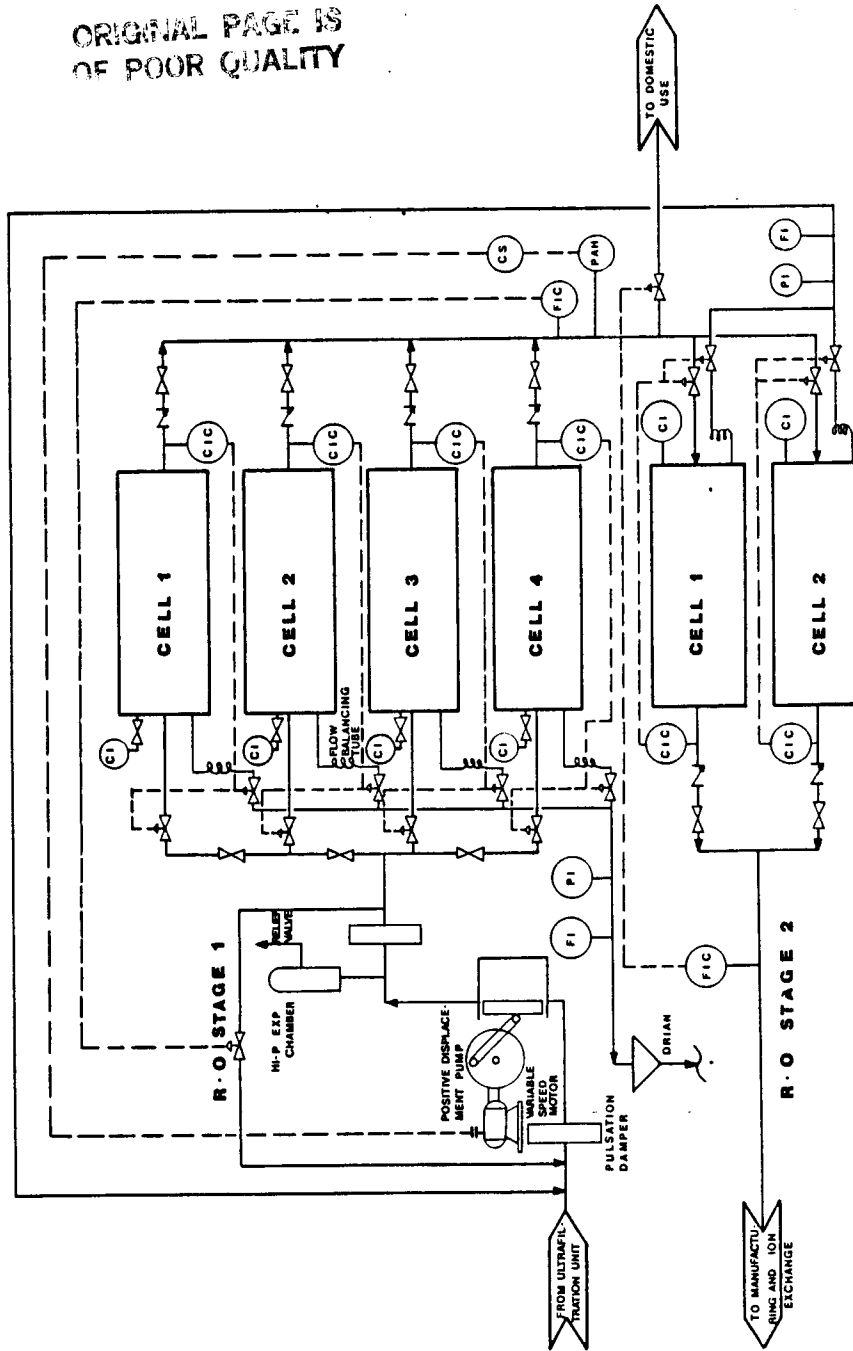
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REVERSE OSMOSIS UNITS 1 & 2

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DISINFECTANTS

TECHNOLOGY REVIEW

CHLORINE

FLUORINE

OZONE

ULTRAVIOLET LIGHT

CHLORINE DIOXIDE

SODIUM HYPOCHLORITE

CHLORINE - effective at low concentrations, forms a residual, and can be manufactured from available brine.



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SELECTION OF DISINFECTANTS

- (1) Ultraviolet light for immediate use of drinking water
and for ion free industrial water.
- (2) Chlorine for all treated water that will be stored,
and pre- and post- chlorination of wastewater.



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OBJECTIVE: MANUFACTURE OF CHLORINE FOR THE
PURIFICATION OF WATER.

METHOD: ELECTROLYSIS OF BRINE IN A DIAPHRAGM
CELL.

OVERALL REACTION



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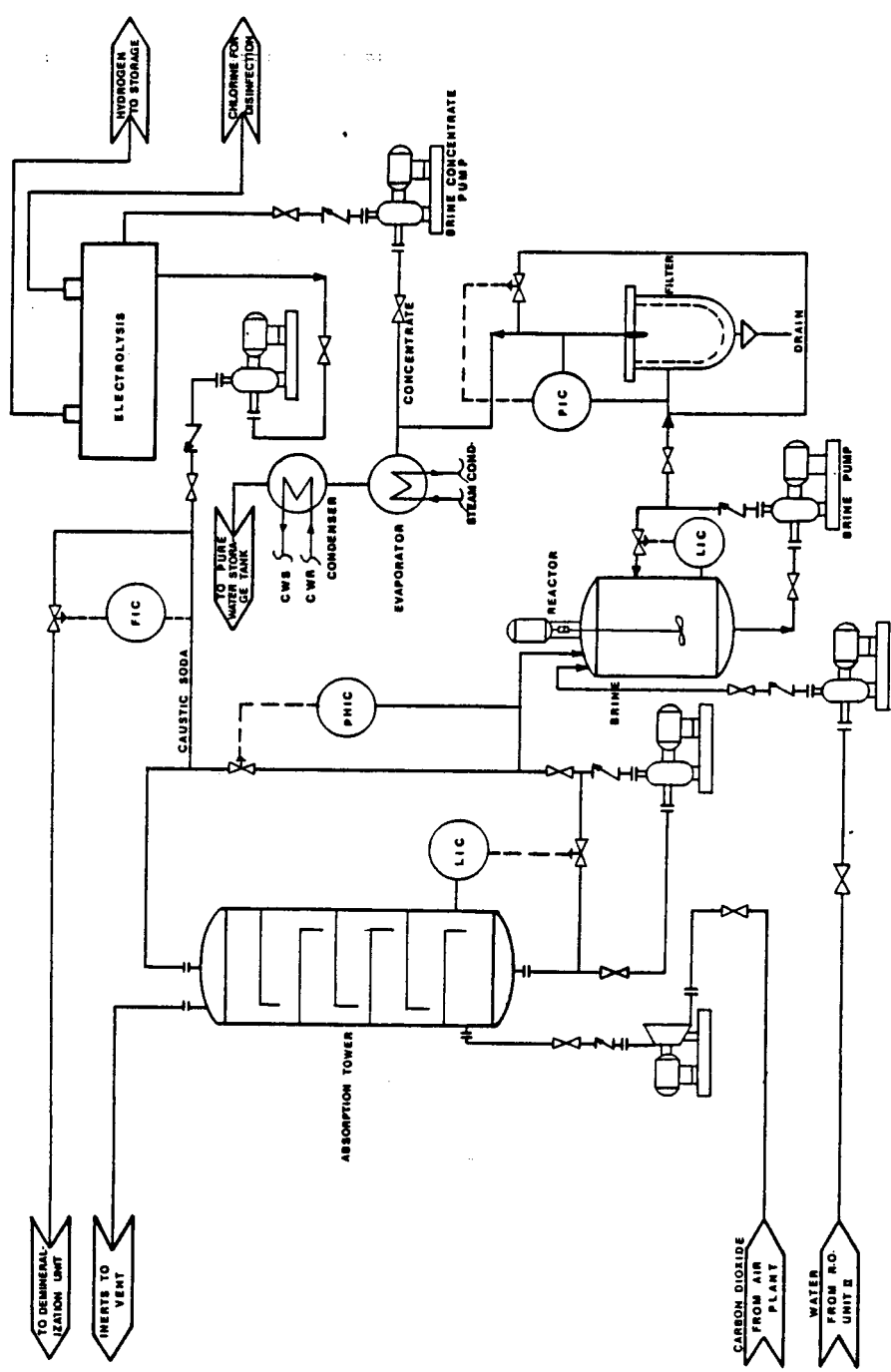
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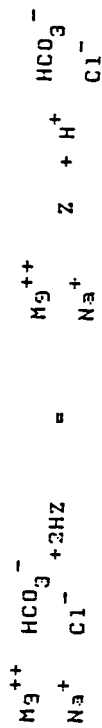
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DISINFECTANT MANUFACTURING UNIT

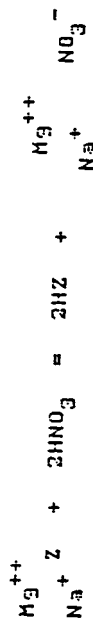


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Thus; CATION EXCHANGE



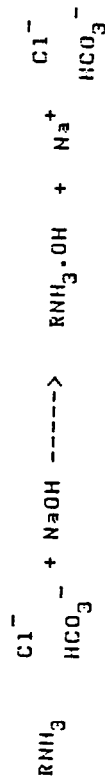
Regeneration



ANION EXCHANGE



Regeneration



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Technical Data Sheet
DOWEX HGR-W Resin

Principal Uses: Best suited for industrial service, such as hot lime zeolite, demineralizing and mixed bed systems. Also for low concentration chrome treatment. Longer life under severe operating conditions and when oxidizing agents are present. Operating temperature to 250°F. (121°C)

General Description: A transparent, water-white cation exchanger produced from a sulfonated copolymer of styrene and divinylbenzene. Strainfree, spheroidal form permits use under conditions restricting application of standard cation exchange resins. Slightly greater density than DOWEX HCR-W.

Density (approx)	54 lb per cu ft (Na Form)
Specific Gravity (true density)	1.30 (Na Form)
Moisture Content (approx)	40-43% (Na Form)
Void Volume (approx)	3.0 gal per cu ft
Wet Mesh Size	Principally 16-40 mesh

Note—Sales Specifications available from Dow Sales Offices.

Regeneration: With sodium chloride (NaCl) at dosages of 6 lb to 15 lb per cu ft for water softening. With either sulfuric or hydrochloric acid for hydrogen cycle use.

Operating Flow Rate: 6 gpm per sq ft for 36 in beds, 2.0 gpm per cu ft for shallower beds; 30 in beds recommended as minimum.

Capacity Range:

Lb NaCl per cu ft (water softening)	Capacity, kg per cu ft as CaCO ₃ (dependent on TDS)
6	23—26
10	28—32
15	30—35

Bed Expansion: 50% max.
@ 9 gpm/ft²
@ 25°C

T.D. Index 140.01 contains operational data applicable to DOWEX HGR-W resin.



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Table 1: Impact of common foulants on resin

Foulant	Cause	Impact
CATION RESIN		
Calcium	Precipitation of calcium sulfate; poor regeneration	Reduced capacity; hardness leakage
Magnesium	Poor regeneration	Reduced capacity; hardness leakage
Iron	In soluble form, is exchanged during service cycle and may then be oxidized and deposited on and within resin beads	Reduced capacity; resin cracking or fragmentation; iron leakage
Aluminum	Exchanged during service cycle but does not elute well during regeneration	Reduced capacity
Barium	Exchanged during service cycle but does not elute well during regeneration. Also, precipitates during sulfuric acid regeneration	Reduced capacity
Silica	Silt in influent	Reduced capacity; poor quality
Oil/grease	Oil-lubricated pumps	Reduced capacity; poor quality
ANION RESIN		
Organics	High ratio of TOC to total anions	Reduced strong-base-resin capacity; poor quality; short service runs; shortened life
Iron	Precipitation	Shortened life; reduced capacity
Silica	Inadequate regeneration caused by concentration of caustic and low caustic temperature	Short runs, poor quality
Aluminum	Precipitation	Reduced capacity; shortened life
Suspended matter	Precipitation	Reduced capacity; poor quality
Oil/grease	Oil-lubricated pumps	Reduced capacity; poor quality

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Capacity and Rinse Requirements
of DOWEX MWA-1 resin

EXHAUSTANT 250 ppm TOTAL ACID	FLOW RATE gpm/ft ³	REGENER- ANT DOSAGE lb/ft ³	TEMPERA- TURE °F	RINSE REQUIRE- MENTS gal/ft ³ to 1M/l	CAPACITY kg/ft ³ to 20,000 l
HCl/H ₂ SO ₄	6	NaOH 7	77 (25 C)	15	22.7
HCl/H ₂ SO ₄	6	5	77	19	22.8
HCl/H ₂ SO ₄	6	3	77	22	21.3
HCl	6	5	77	17	22.2
HNO ₃	6	5	77	15	24.3
H ₂ SO ₄	6	5	77	20	22.8
HCl/H ₂ SO ₄	6	5	54 (12 C)	22	20.3
HCl	6	5	54	17	20.3
H ₂ SO ₄	6	5	54	22	21.9
HCl/H ₂ SO ₄	3	5	77 (25 C)	16	23.1
HCl/H ₂ SO ₄	4.5	5	77	17	22.9
HCl/H ₂ SO ₄	9.0	5	77	16	22.9
HCl/H ₂ SO ₄	6	NH ₄ OH	77	22	20.0
HNO ₃	6	4.35	77	22	22.4
HCl/H ₂ SO ₄	6	Na ₂ CO ₃ 6.6	77	25	19.6



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Technical Data Sheet DOWEX SBR-P Resin

Principal Uses: A highly porous anion exchanger for use in all types of deionizers, performing best on waters having a high percentage of weak acids (CO_2 and SiO_2) to total anions. Also used in ion exchange waste treatment processes. Operating temperature below 120°F, (49°C).

General Description: A styrene type, strongly basic anion exchanger produced from styrene and divinylbenzene, and containing quaternary ammonium groups; spherical form.

Density (chloride form) (approx) 43 lb per cu ft
Specific Gravity

(true density) 1.09

Moisture Content 53-60%

Void Volume (approx) 3.0 gal per cu ft

Mesh Size Principally 16-40 mesh

Note — Sales Specifications available from Dow Sales Offices.

Regeneration: With sodium hydroxide (NaOH) at dosages of 3.5 lb per cu ft or higher, at temperatures ranging from 75°F (24°C) to 120°F (49°C).

Operating Flow Rate: 6 gpm per sq ft for 36 in beds, 2.0 gpm per cu ft for shallower beds; 30 in beds recommended as minimum.

Capacity Range:

lb NaOH per cu ft	kg per cu ft as CaCO_3 Acid removing capacity (HCl : H_2SO_4)
3.5	9.0 — 9.5
5.0	11 — 11.5
7.5	12.5 — 13

Bed Expansion: 80% max.
@ 4 gpm/ft²
@ 25°C

112 For further information — see I.D. Index 230.01



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How Impurities in Water Are Expressed

In the U.S., impurities are usually expressed in terms of calcium carbonate (CaCO₃) as grains per gallon (gpg), equivalents per million (epm), or parts per million (ppm). Foreign systems expressing impurities are:

- 1 English degree (°Clark) = 1 grain CaCO₃ per British Imperial gallon water.
- 1 French degree = 1 part CaCO₃ per 100,000 parts water.
- 1 German degree = 1 part Calcium Oxide (CaO) per 100,000 parts water.

CONVERSIONS BETWEEN SYSTEMS

	Grains per U.S. Gallon (gpg)	Parts per Million (ppm)	Equiv. per Million* (epm)	English Degrees (°Clark)	Parts per 100,000 (French Degrees)	German Degrees
1 grain per U.S. gallon	1.0	17.1	.343	1.2	1.71	.958
1 part per 100,000	.583	10.0	0.2	0.7	1.0	0.55
1 part per million	.058	1.0	.02	.07	0.1	.055
1 equivalent per million*	2.92	50.0	1.0	3.5	5.0	2.8
1 English Degree (°Clark)	.833	14.3	.286	1.0	1.43	0.8
1 French Degree	.563	10.0	0.2	0.7	1.0	0.55
1 German Degree	1.04	17.9	.357	1.24	1.79	1.0

*1 equivalent per million = 1 milliequivalent per liter.

CONVERSION FACTOR USED IN ION EXCHANGE

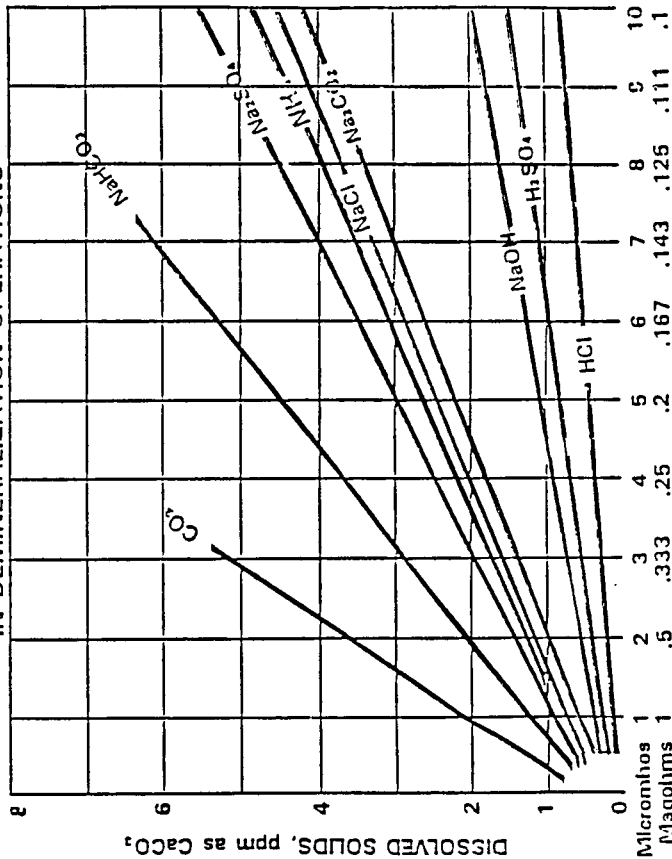
Ion	Factor	Ion	Factor
Ca	X 2.5 = CaCO ₃	NO ₃	X .81 = CaCO ₃
Mg	X 4.1 = CaCO ₃	HCO ₃	X .82 = CaCO ₃
Na	X 2.18 = CaCO ₃	PO ₄	X 1.56 = CaCO ₃
K	X 1.28 = CaCO ₃	*CO ₃	X .84 = CaCO ₃
SO ₄	X 1.04 = CaCO ₃	*CO ₂	X 1.14 = CaCO ₃
Cl	X 1.41 = CaCO ₃	*SiO ₂	X .83 = CaCO ₃



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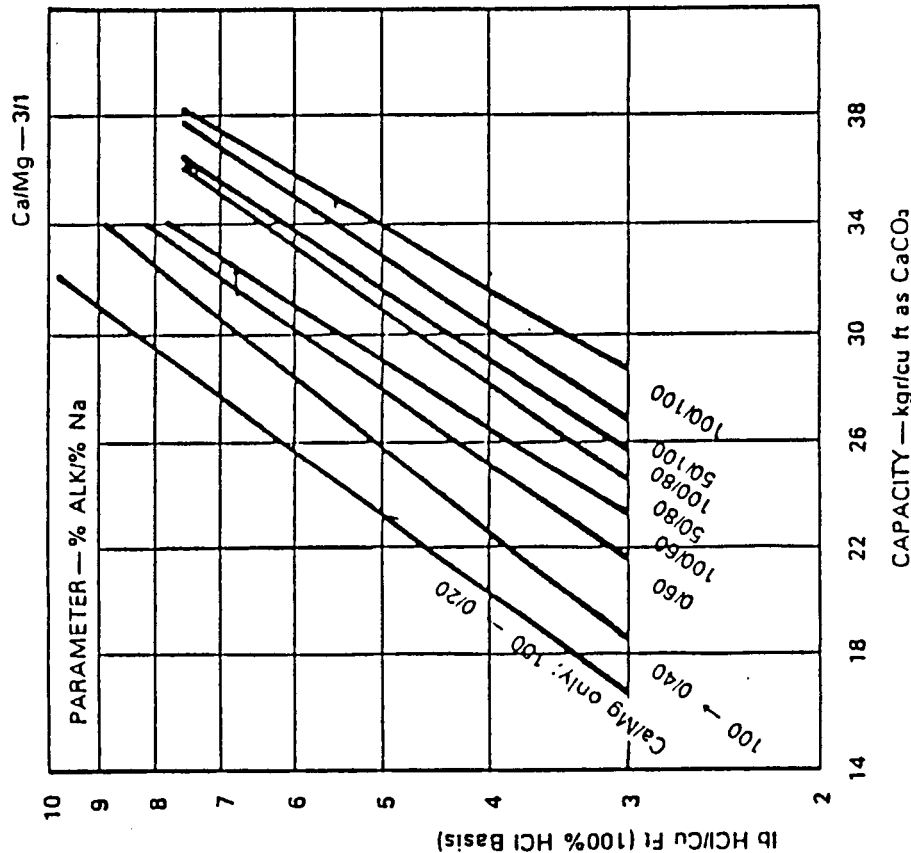
RELATIONSHIP BETWEEN
DISSOLVED SOLIDS AND CONDUCTANCE
IN DEMINERALIZATION OPERATIONS



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Capacity Rating of DOWEX Cation Exchangers Corrected for Leakage



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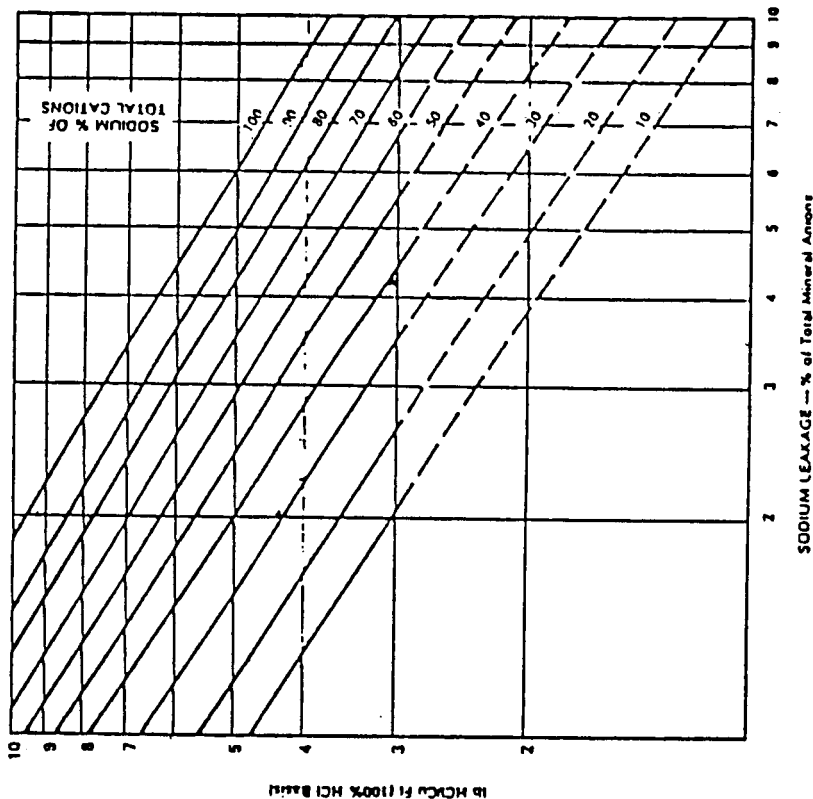
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Sodium Leakage from HCl Regenerated DOWEX
Cation Exchange Resins

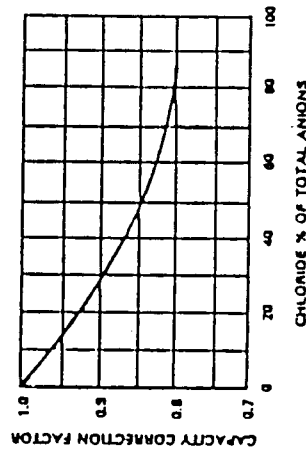
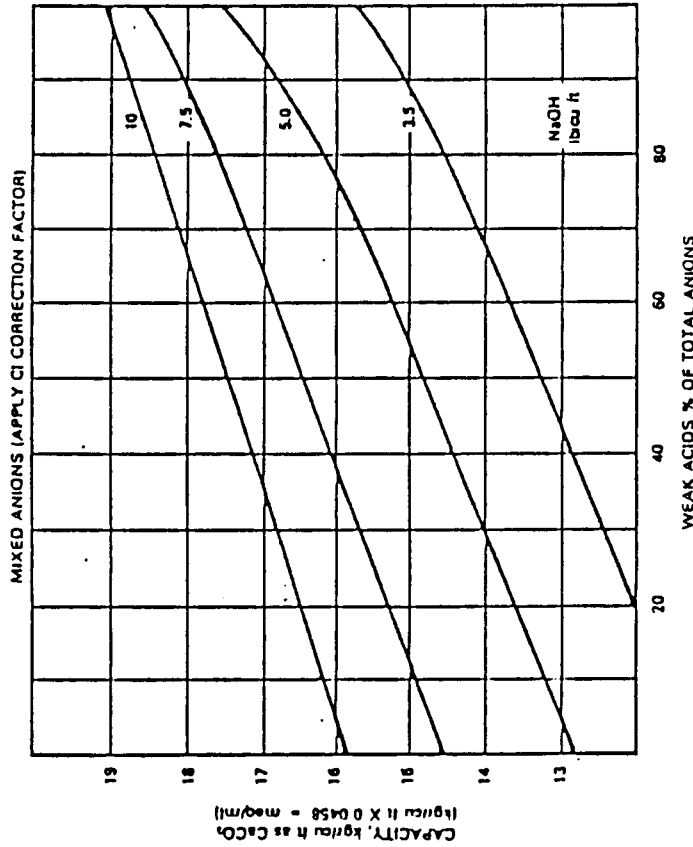


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Operating Exchange Capacity of DOWEX SBR-P Resin (120 F (49 C) Regenerating Temperature, 77 F (25 C) Operating Temperature)



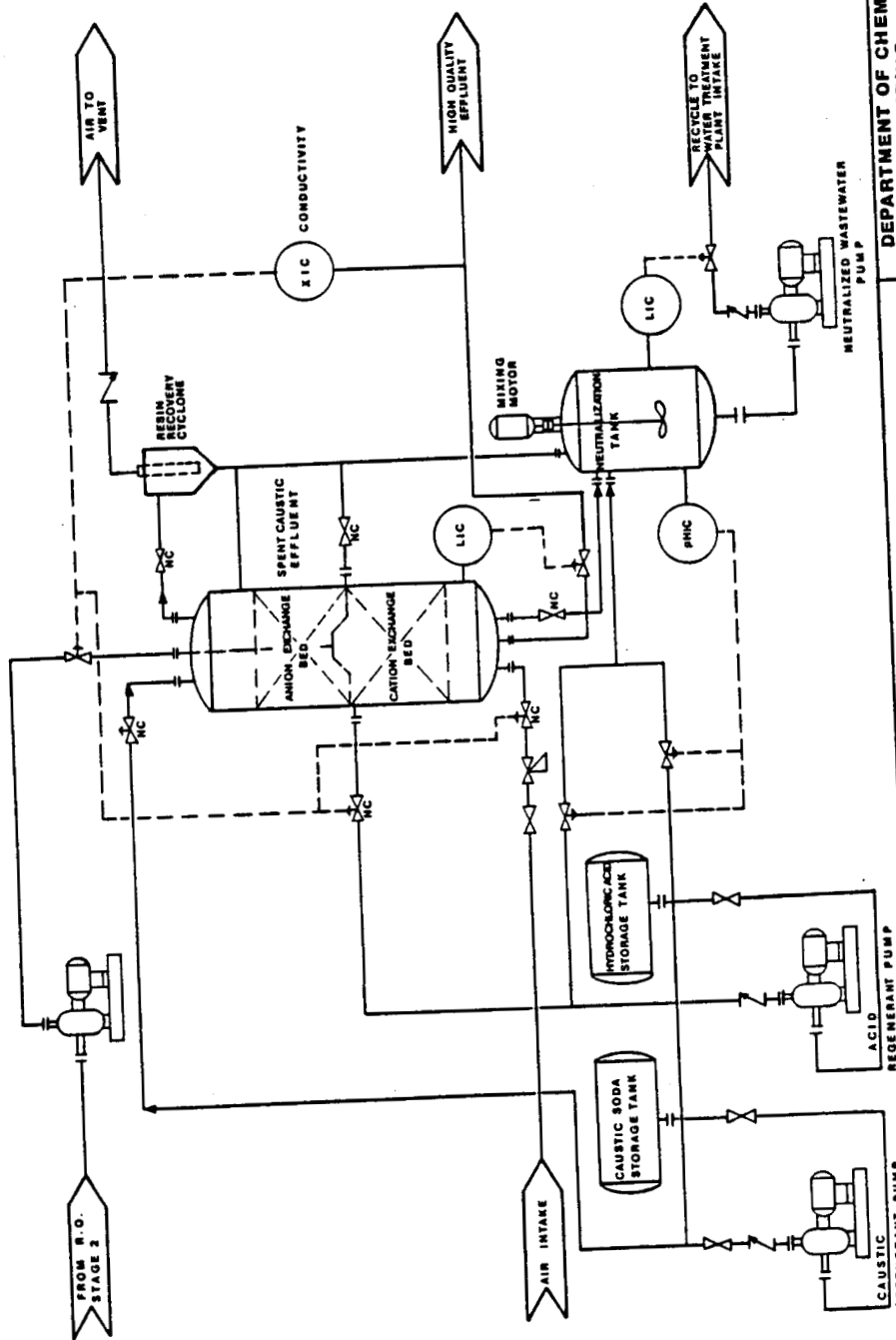
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DEMINERALIZATION UNIT

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WASTEWATER CONSTITUENTS

Characteristic	Sources
Physical properties:	
Color	Domestic and industrial wastes, natural decay of organic materials
Odor	Decomposing wastewater, industrial wastes
Solids	Domestic water supply, domestic and industrial wastes, soil erosion, inflow-infiltration
Temperature	Domestic and industrial wastes
Chemical constituents:	
Organic:	
Carbohydrates	Domestic, commercial, and industrial wastes
Fats, oils, and grease	Domestic, commercial, and industrial wastes
Pesticides	Agricultural wastes
Phenols	Industrial wastes
Proteins	Domestic and commercial wastes
Surfactants	Domestic and industrial wastes
Others	Natural decay of organic materials
Inorganic:	
Alkalinity	Domestic wastes, domestic water supply, groundwater infiltration
Chlorides	Domestic water supply, domestic wastes, groundwater infiltration, water softeners
Heavy metals	Industrial wastes
Nitrogen	Domestic and agricultural wastes
pH	Industrial wastes
Phosphorus	Domestic and industrial wastes, natural runoff
Sulfur	Domestic water supply, domestic and industrial wastes
Toxic compounds	Industrial wastes
Gases:	
Hydrogen sulfide	Decomposition of domestic wastes
Methane	Decomposition of domestic wastes
Oxygen	Domestic water supply, surface-water infiltration
Biological constituents:	
Animals	Open watercourses and treatment plants
Plants	Open watercourses and treatment plants
Protozoa	Domestic wastes, treatment plants
Viruses	Domestic wastes

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DESIGN ASSUMPTIONS

Flowrate 10,000 gallons/day

Gravity = 3/8 earths gravity

Stokes law applies to settling

Return sludge concentration is 7000 mg/L

Temperature 20° C



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* All values except settleable solids are expressed in mg/L.

CONSTITUENT

*** CONCENTRATION**

SOLIDS, TOTAL

720

DISSOLVED

505

SUSPENDED

222

SETTLEABLE SOLIDS

10 mL/L

BOD (Biochemical Oxygen

222

Demand)

TEMPERATURE 20° C



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EFFLUENT STANDARDS

CONSTITUENT

CONCENTRATION

SUSPENDED SOLIDS

20 - 30 mg/L

BOD

15 - 25 mg/L



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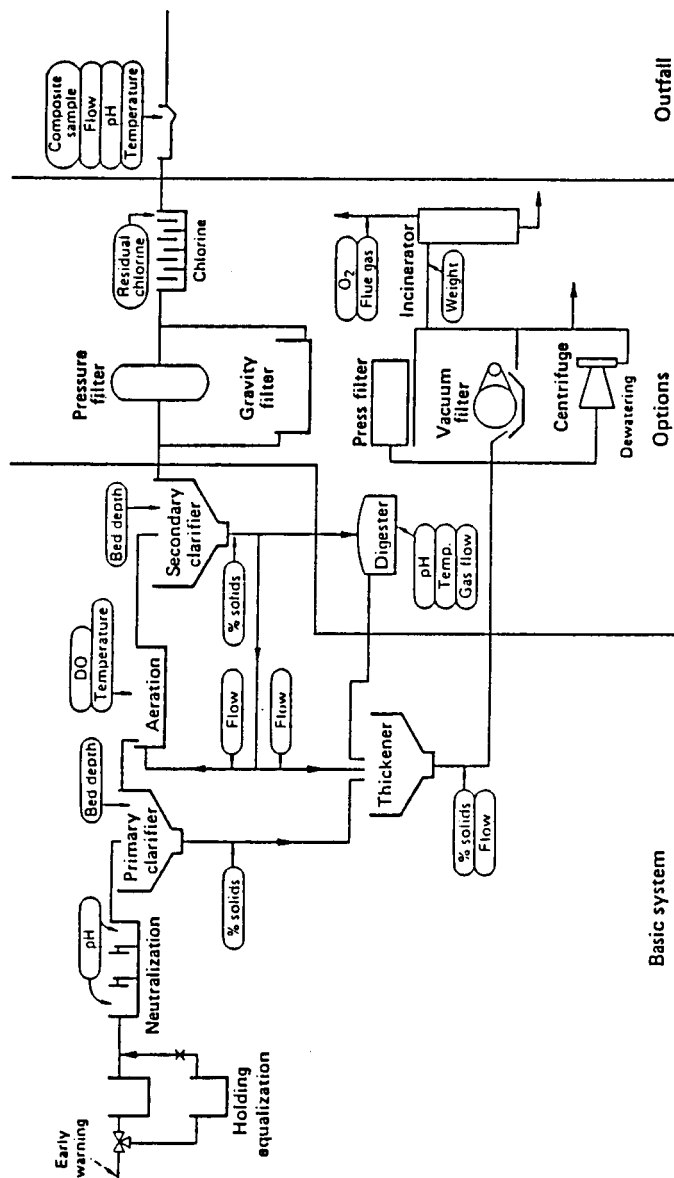
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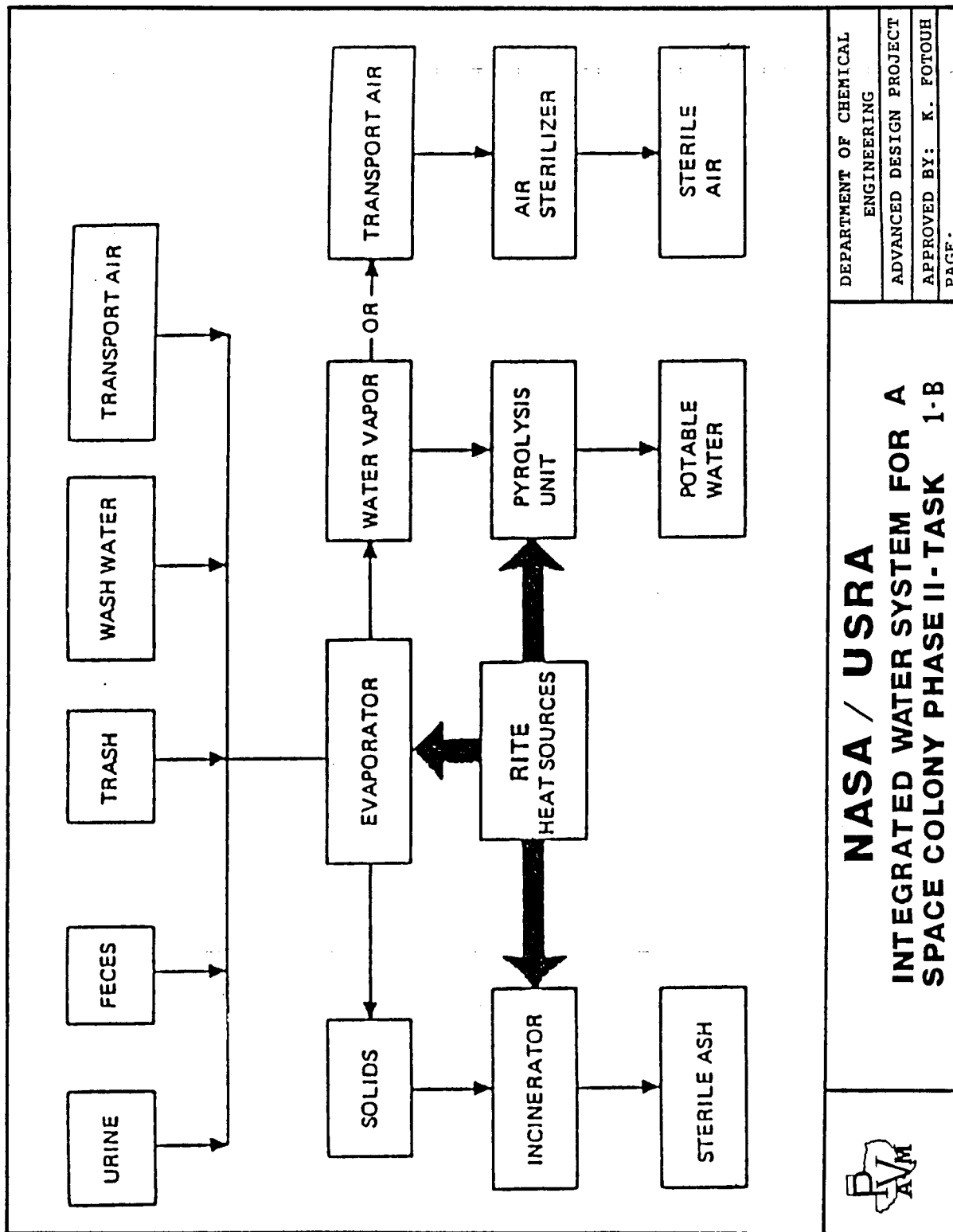


Typical wastewater treatment plant showing instrumentation described in text



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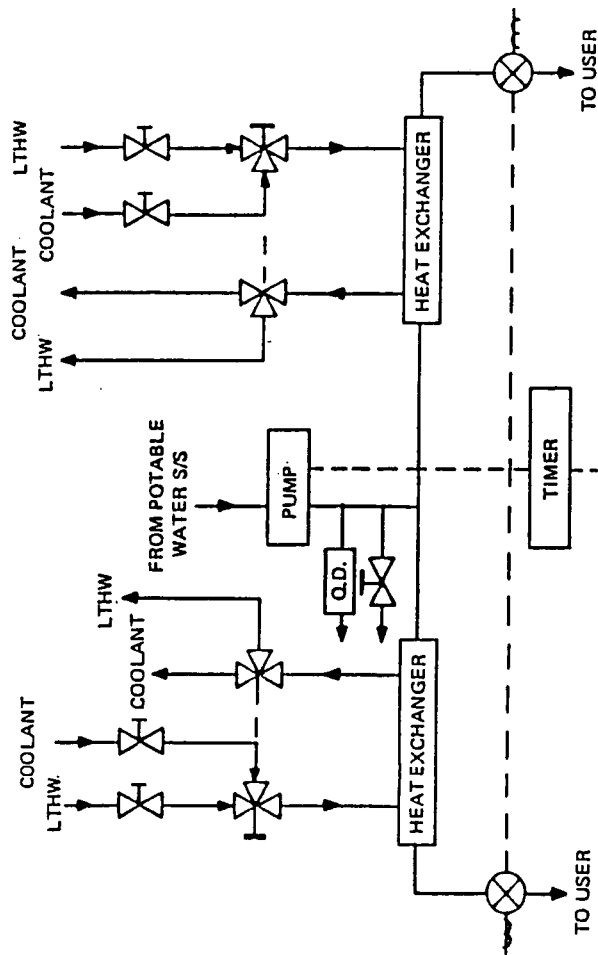


Figure Potable Water Dispensing Schematic



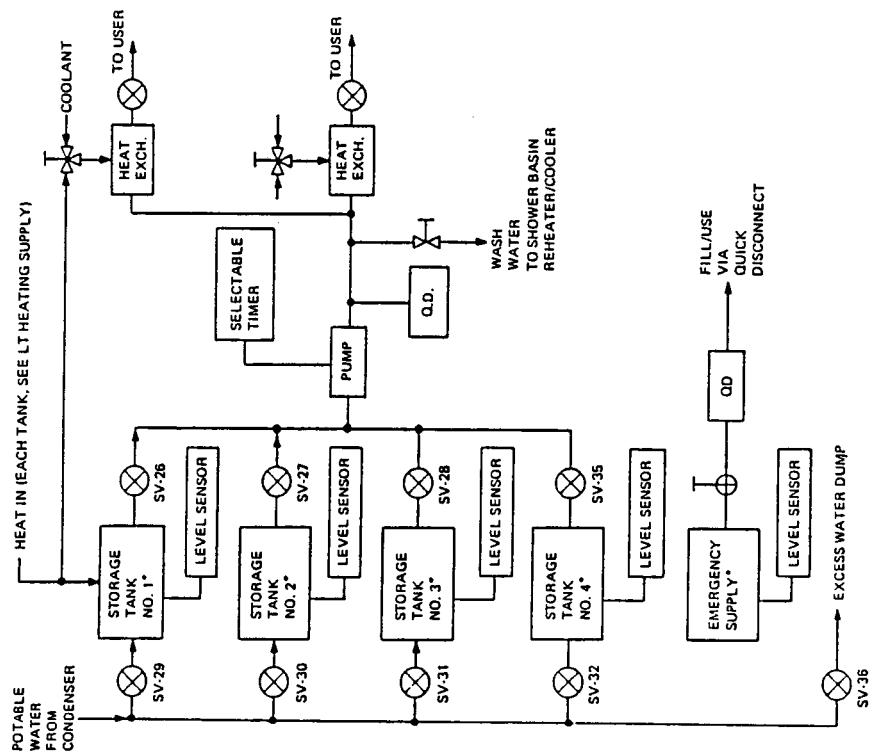
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*ELECTRIC HEATER PROVIDED IN EACH TANK FOR EMERGENCY STERILIZATION

Figure Potable Water Storage/Dispensing Functional Schematic



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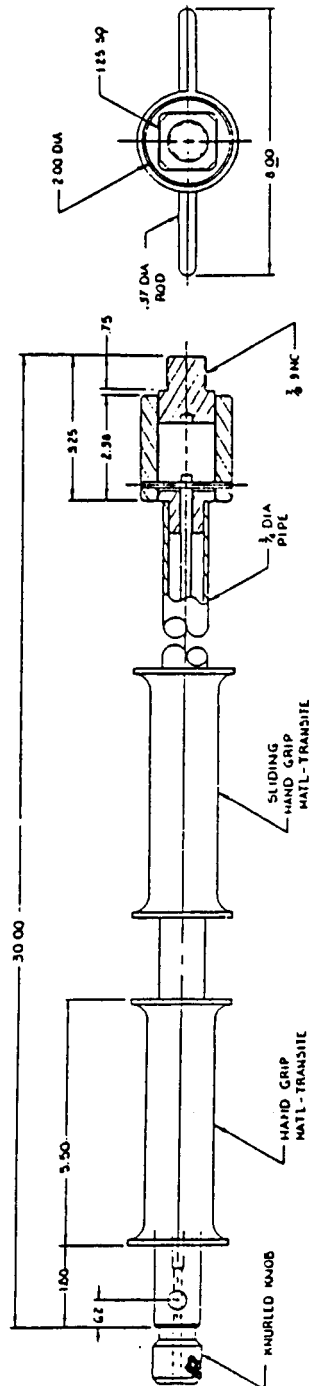
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NOTES:
1 ALL DIMS ARE FOR REF ONLY
2 MATL STAINLESS 316 EXCEPT AS
NOTED.

Figure Rite Heat Source Handling Device



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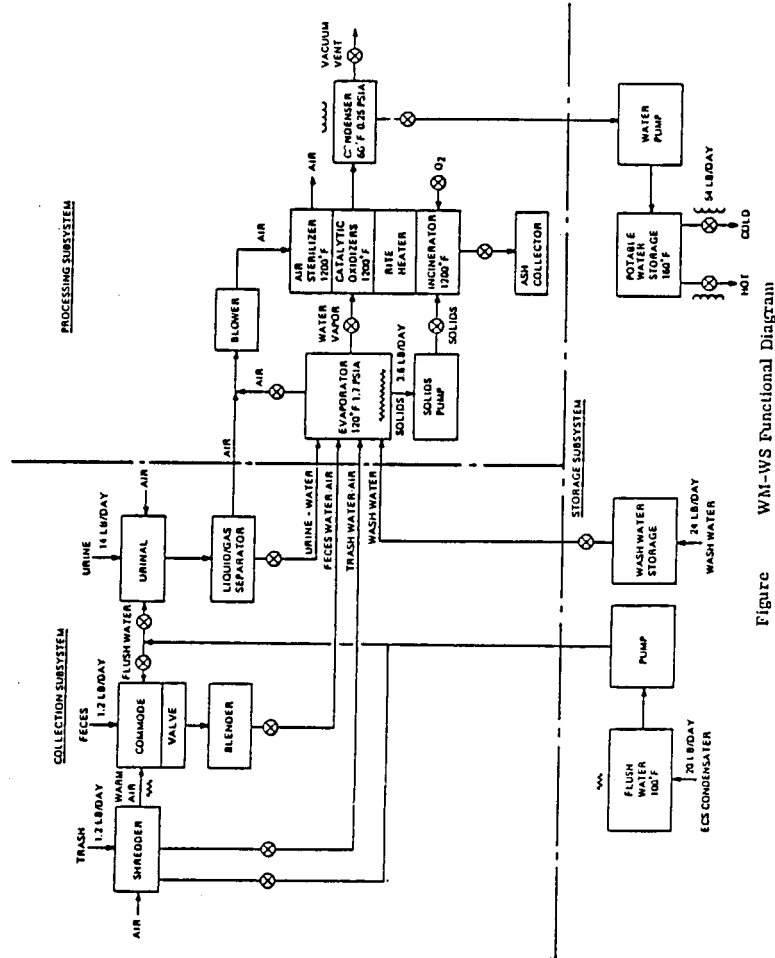


Figure WM-WS Functional Diagram

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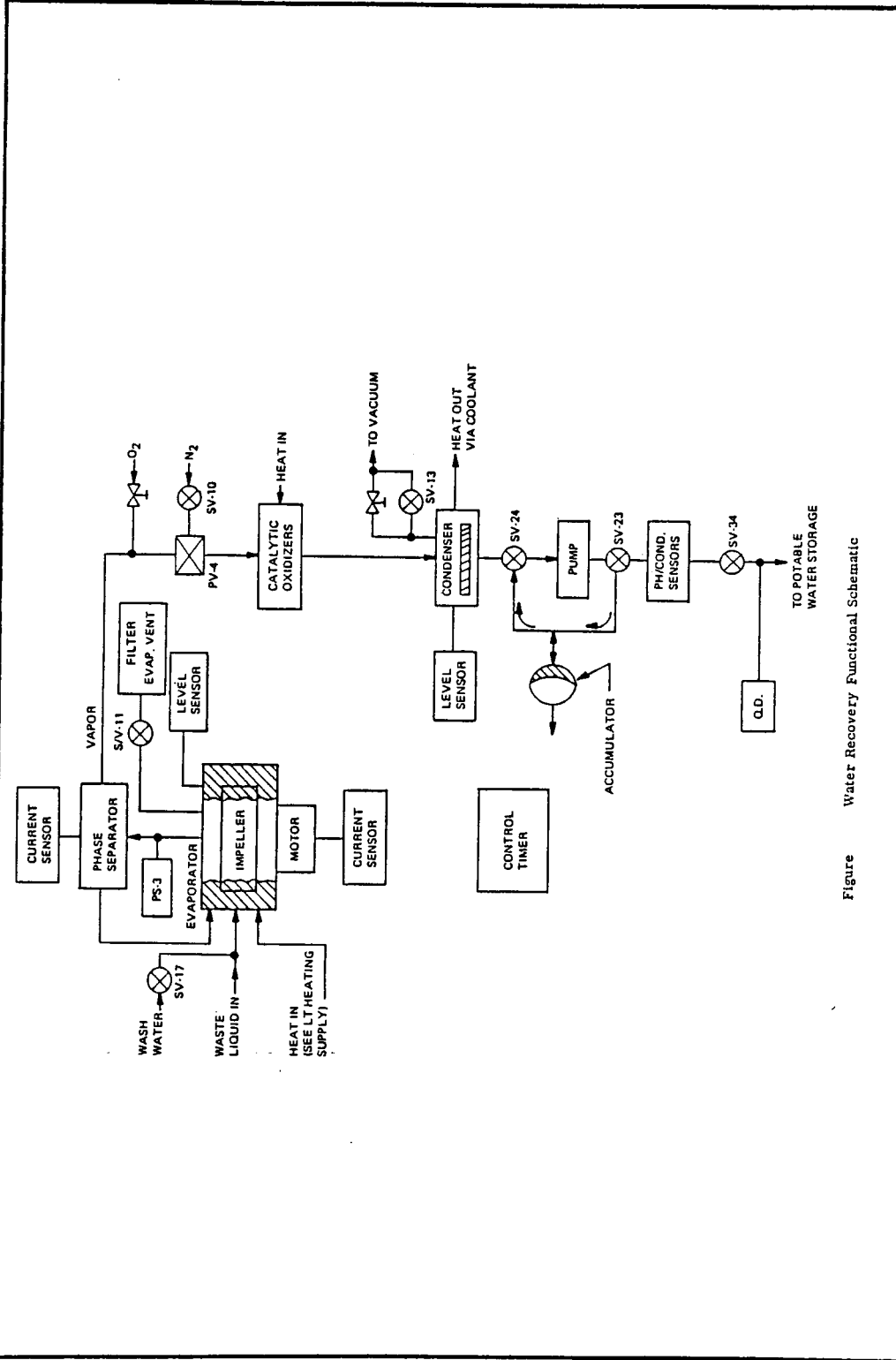


Figure Water Recovery Functional Schematic



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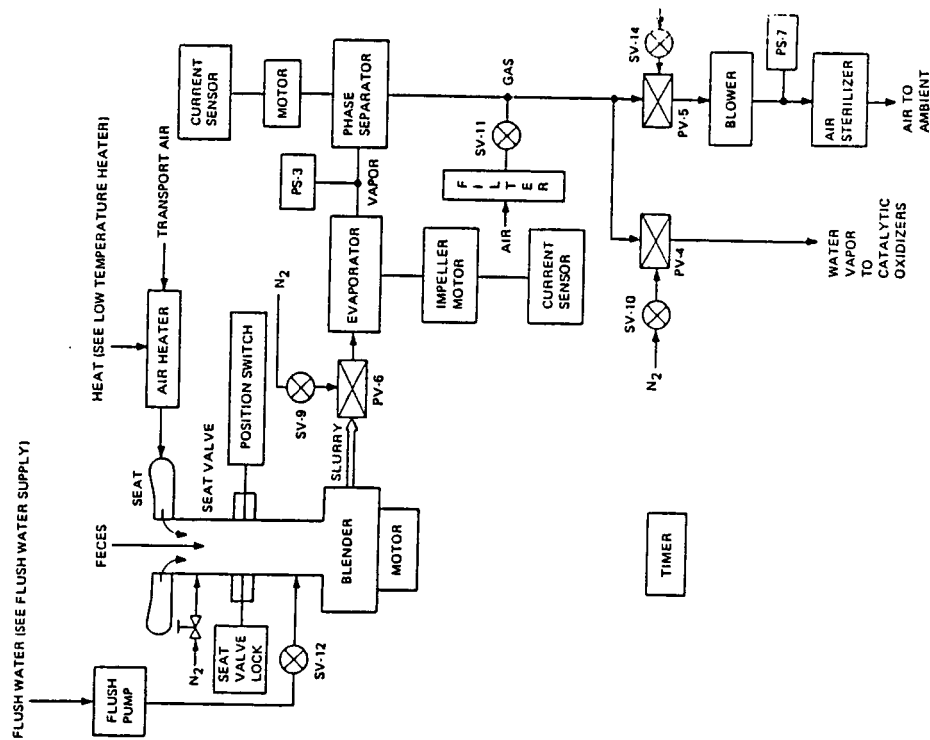


Figure Feces Collection Functional Schematic



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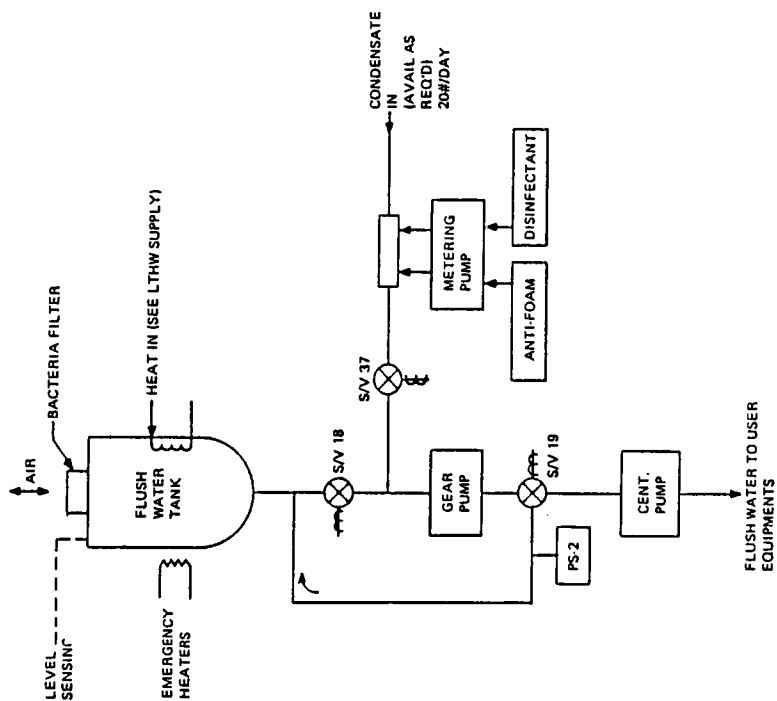


Figure Flush Water Supply Functional Schematic

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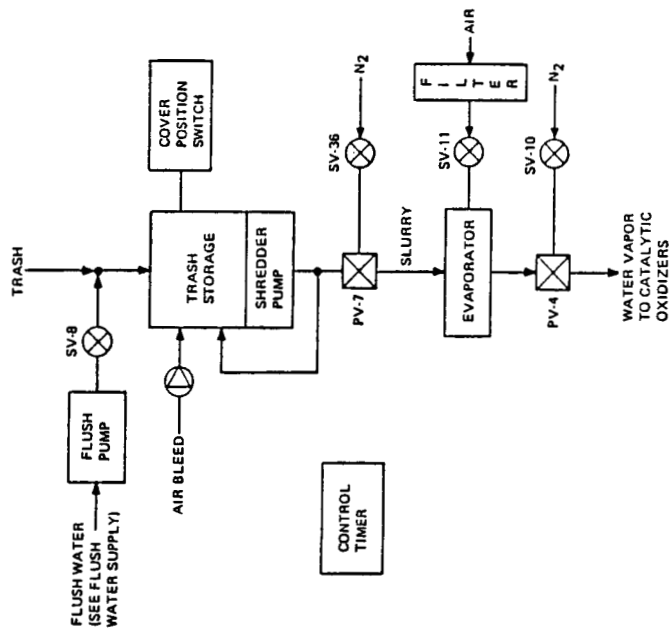


Figure Trash Collection Functional Schematic



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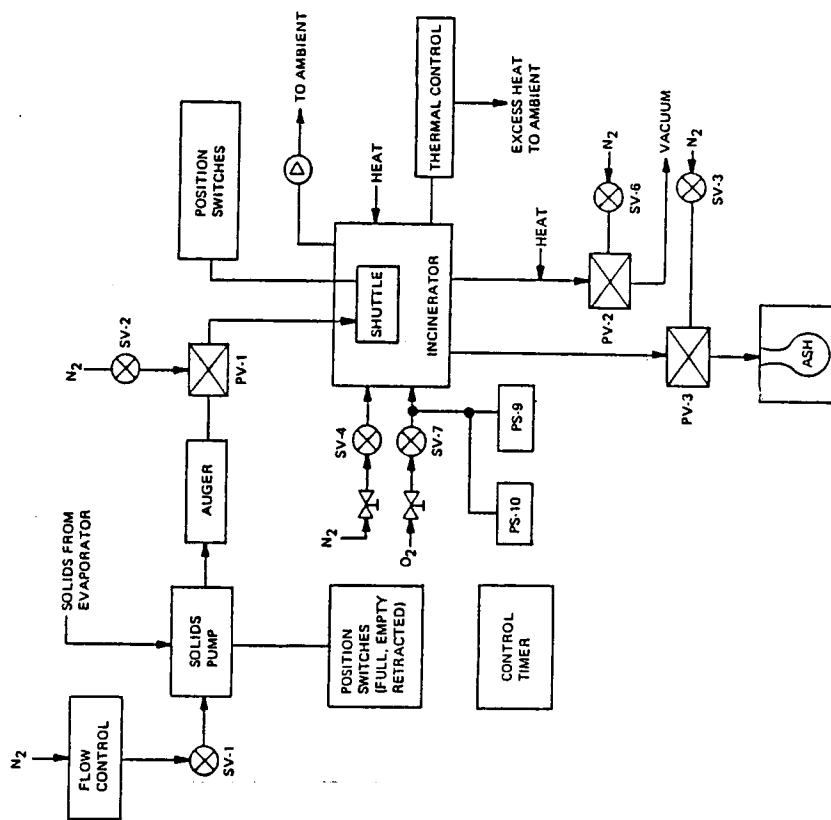


Figure Solids Pump and Incineration Functional Schematic



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TRANSIT CAPSULE HARDWARE
836 WATTS Pu 238

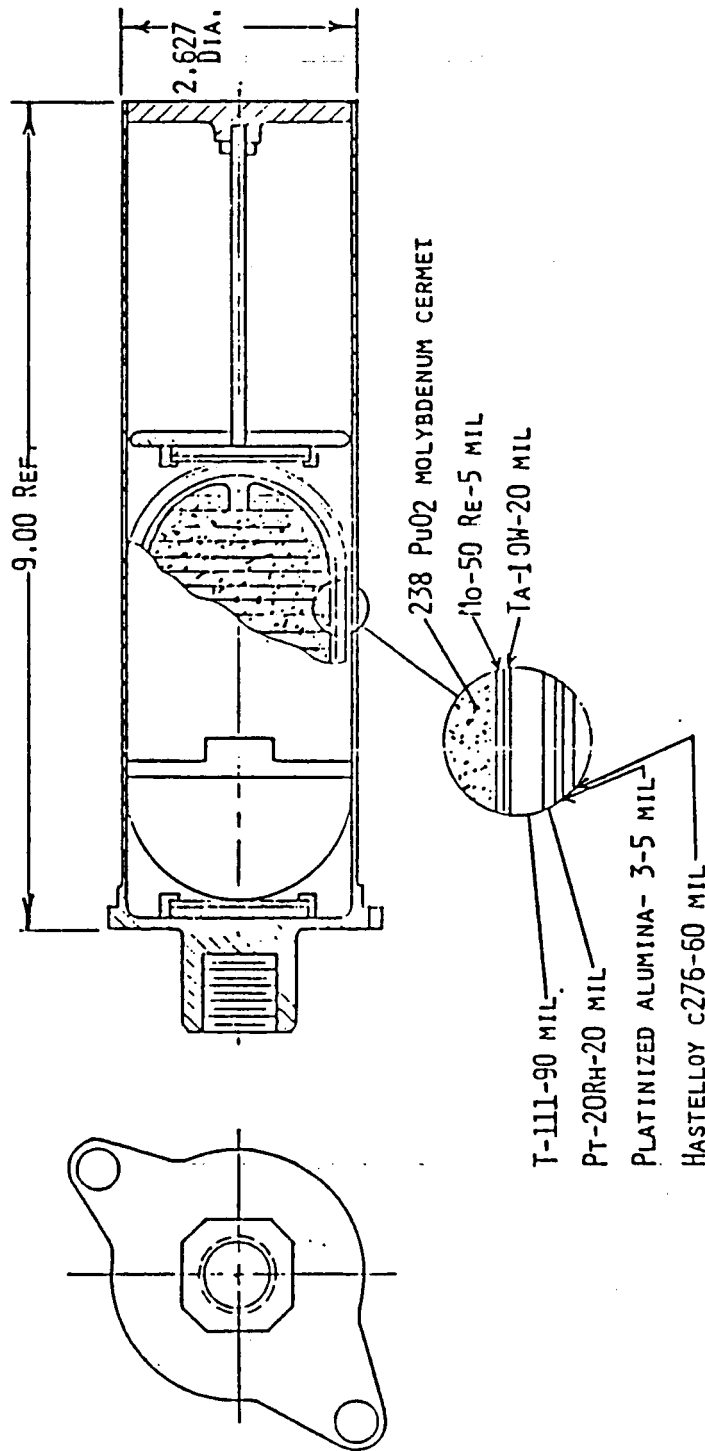


Figure Rite II Heat Source Layout Drawing



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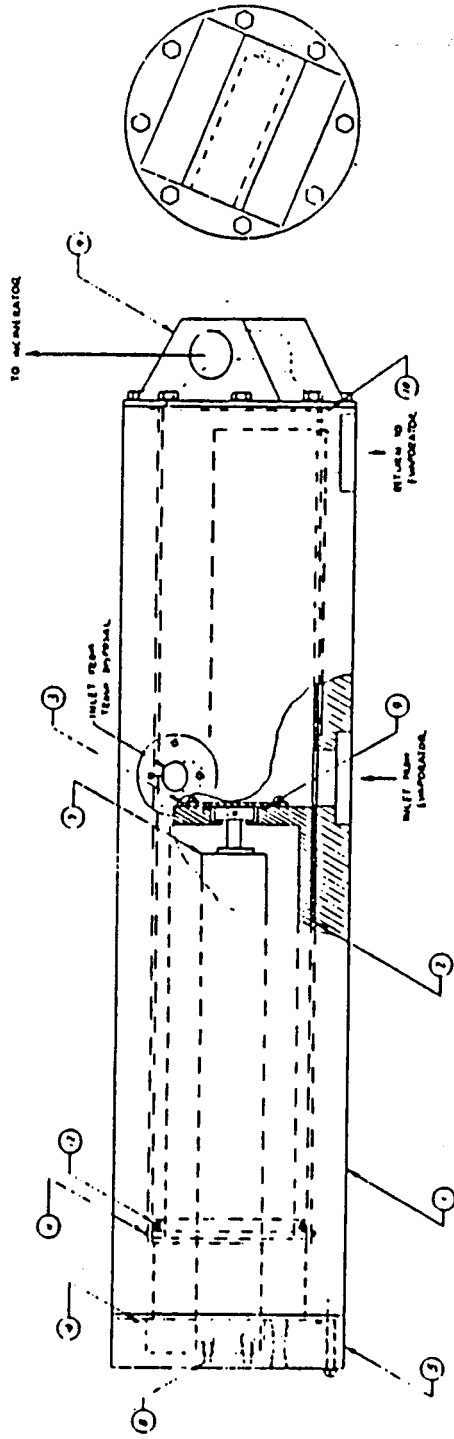


Figure Solids Pump



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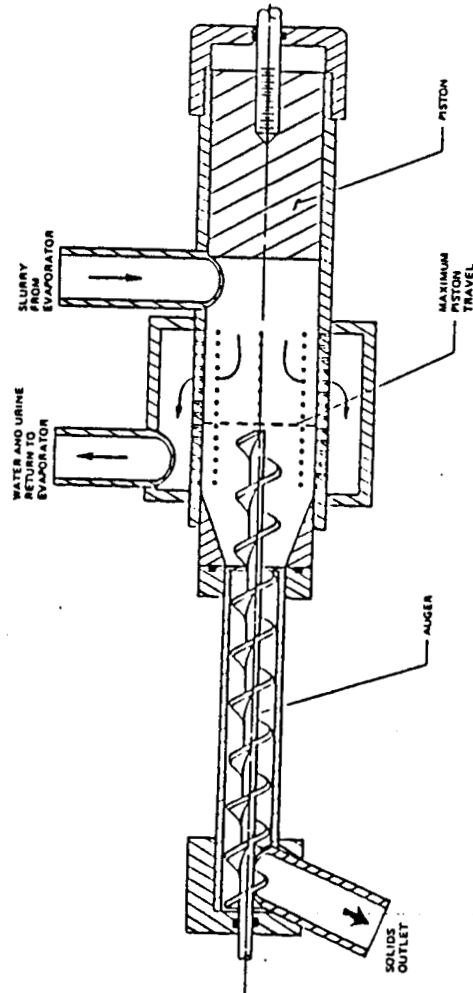


Figure Solids Pump Development Model with Auger, Schematic



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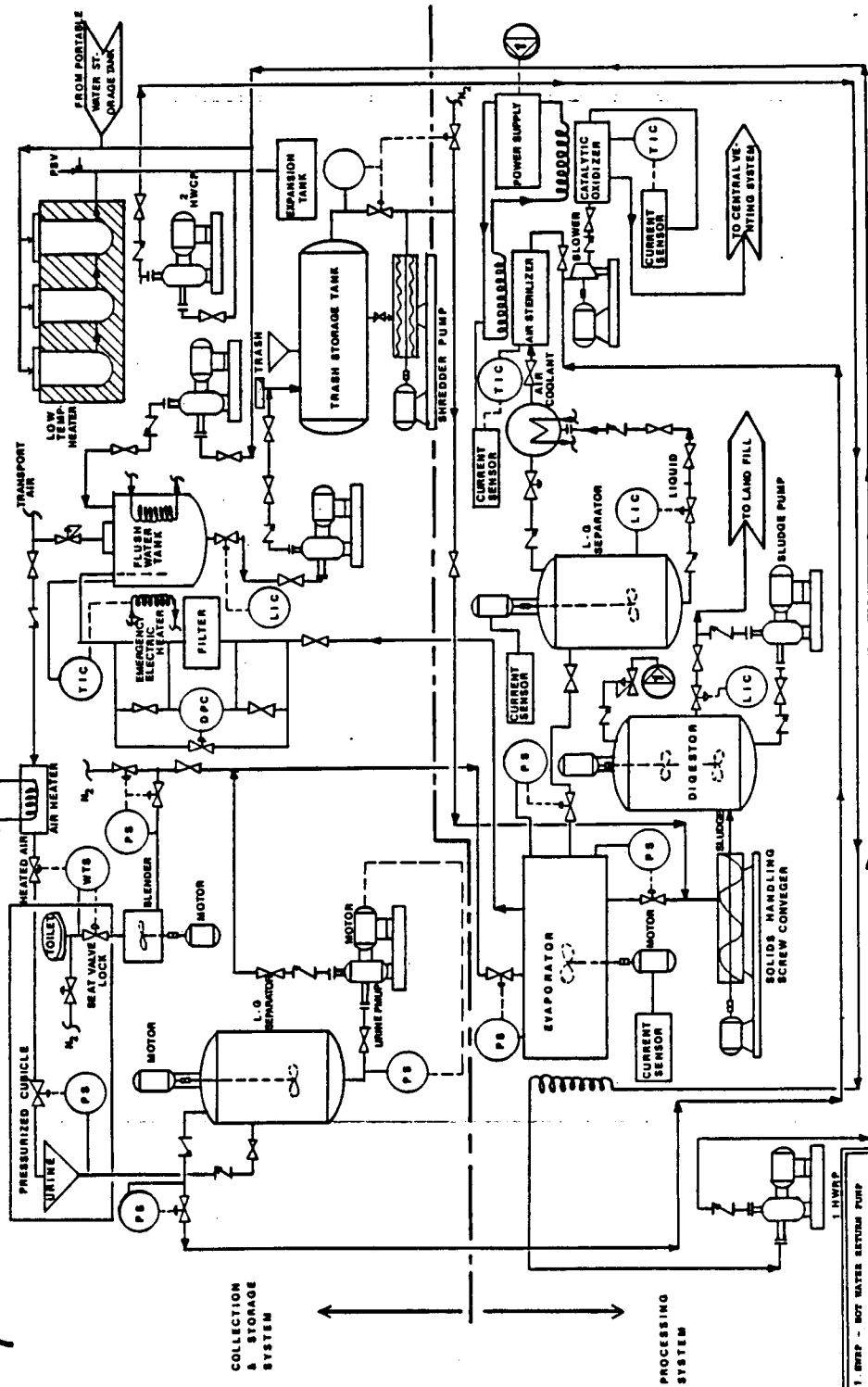
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DOMESTIC WASTE WATER MANAGEMENT

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COMPUTATION SHEET

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Listed by.....	Project: INTEGRATED WATER SYSTEM FOR A SPACE COLONY	Est. No.....
Checked by.....	Phase II - TASK I - B	Sheet 2 of 2
Cont. No.....	Client: NASA/USRA	Date.....
	Location: MARS	

SUMMARY OF TECHNIQUES FOR REMOVING METALS (CONTINUE)

Precipitation					
Thioacetamide		HCl	ppb (varies)	0.75 8.0	Cd, Cu, Pb Cr, Hg, Zn, Mn
Metal sulfides	Cooling tower blow-down	HCl	15-200 ppm	2.3	Cr, Mn, Sr, Cu, Ni, Co
Dibromo-oxine	Seawater	Acetone	ppb	8.0	Cu, Zn, Co, Mn, Pb, Cr
Potassium Ferrocyanide	Electroplating solutions	Activated carbon	-	-	Pb, Sn, Cd, Zn, Fe, Ni, Co
Dialkyldithio- carbamates	Process streams	-	70 ppm	4.2	Zn, Cu, Fe
Oxalate or sulfate	Radioactive rinse water	-	40 ppb	-	Sr
Polyelectrolytes	Process solvents	Polygalacturonic & alginate acids	mg/l	4.0-4.5	Cu, Cd, Zn, Ni, Cr
Aluminum sulfates	Industrial & municipal water	-	0.20 mg/l	6.8-7.0	Pb, Cu, Cr, Cd, Zn, Ni
Lime	Industrial & municipal water		0.26 mg/l	9.6	Mn & others
Carbonates	Industrial & municipal water	CaO or NaOH	0.2 mg/l	9.5	Mn & others
Hydroxides	a. Industrial & municipal water	Ca(OH) ₂	100s of mg/l	1-0.5	Pb, Cu, Cd, Ni, Co, Mn, Zn
	b. Seawater	Li(OH) ₄	24 µg/l	0.0	Mn
	c. Seawater	Mg(OH) ₂	60 µg/l	-	Cr
	d. Process solutions	Mg(OH) ₂ + Ca(OH) ₂	g/l	-	Sr, Pb
	e. Municipal & Industrial water	NaOH	100s of mg/l	1-0.5	Mn & others

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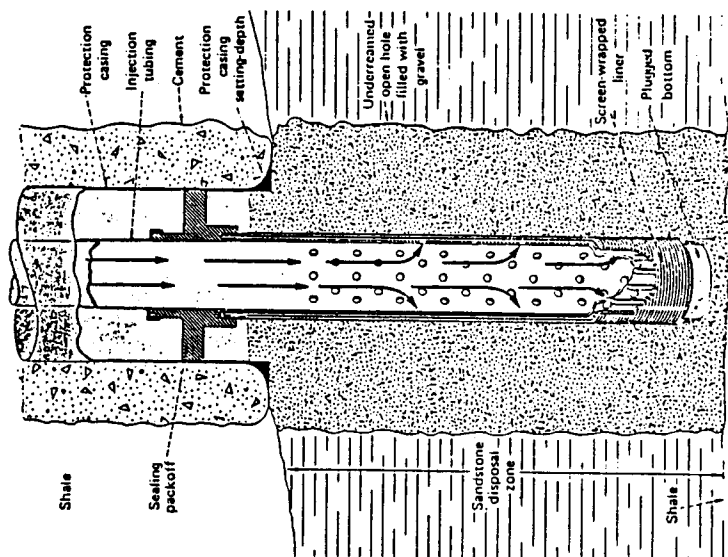
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Checked by	Client PHASE II - TASK 1-B NASA/USRA	Sheet 1 of 2
Cont. No.	Location MARS	Date

SUMMARY OF TECHNIQUES FOR REMOVING METALS

Method	Source	Reagents	Concentration	pH Range	Ions
Extraction	Water	Ammonium pyrrolidone dithiocarbamate, methyl iso butyl ketone, chloroform	Several ppb	4.5-8	Cu, Pb, Ni, Zn, Cd, Co, Mn, Mo, V
Foam separation	Industrial processes	N ₂ , surfactant	0.06 g/l & lower	5.5-8	Ni, Cr, Co, Sr
Autoclaving	Biological samples	Steam	ppb	—	Ti, Cr, Cu, Pb, Mn, Sn
Adsorption on alumina	Radioactive rinse water	—	Up to 1 x 10 ³ moles/l	8.0	Sr
Aeration	Municipal & industrial water supplies	KMnO ₄ , activated carbon	0.2 mg/l	—	Mn, Fe
Manganese zeolite bed	Municipal & industrial water	KMnO ₄ , anthracite	0.2 mg/l	—	Mn, Fe
Ultraviolet radiation & magnetic field	Seawater, freshwater, industrial streams	—	—	—	All
Paper chromatographic separation	—	Mixture of chloroform, methanol, acetone, isopentanol & formic acid, INDA HCl	ppb	—	Cu, Pb, Cd, Bi, Hg, Mn, Co, Ni, Cu, Zn, Fe
Rotating electrodes	Process streams, seawater	—	—	—	All
Biological	a. Acid mine waters b. Municipal & industrial water streams	Yeasts, sulfur, glucose Bacteria	10s of mg/l	3.5	Cu Fe, Mn
Ion Exchange Chelex-100	Sea & fresh water, process waters	HCl	Varies	5-6	Cu, Pb, Cr, Ni, Zn, Co, Cd, Mn
Chitosan	Salt water	EDTA	ppb (varies)	—	Mn, Ti, Cr, Pb
Amberlite	Process liquid	Eluant	Varies	—	Cd, Co, Cu, Pb, V, Zn, Ni
Titanium arsenate	—	NH ₄ NO ₃ , HNO ₃	Varies	—	Pb, Co, Cd, Sr, Zn, Mn, Ni, Co
Permutit-S1005	Seawater	Eluant	ppb	7.0 5.0 (Mn, Cr) 6.0 (V) 9.0 (Mn)	Cd, Co, Cu, Pb, Ni, Zn, Cr
DeAcidite FF + dibromo-oxine	Seawater, cooling tower blowdown	HCl or H ₂ SO ₄	ppb 200 ppm	—	Co, Zn, Cr
Zeo-Karb 225	Process streams, rain water	H ₂ SO ₄	ppb	—	Sr
Dowex	Water, process streams	Eluant	100 ppm	Varies	Fe, Co, Mn, Cd, Cr, Cu, Zn, Pb

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Completion for disposal into
sandstone formation

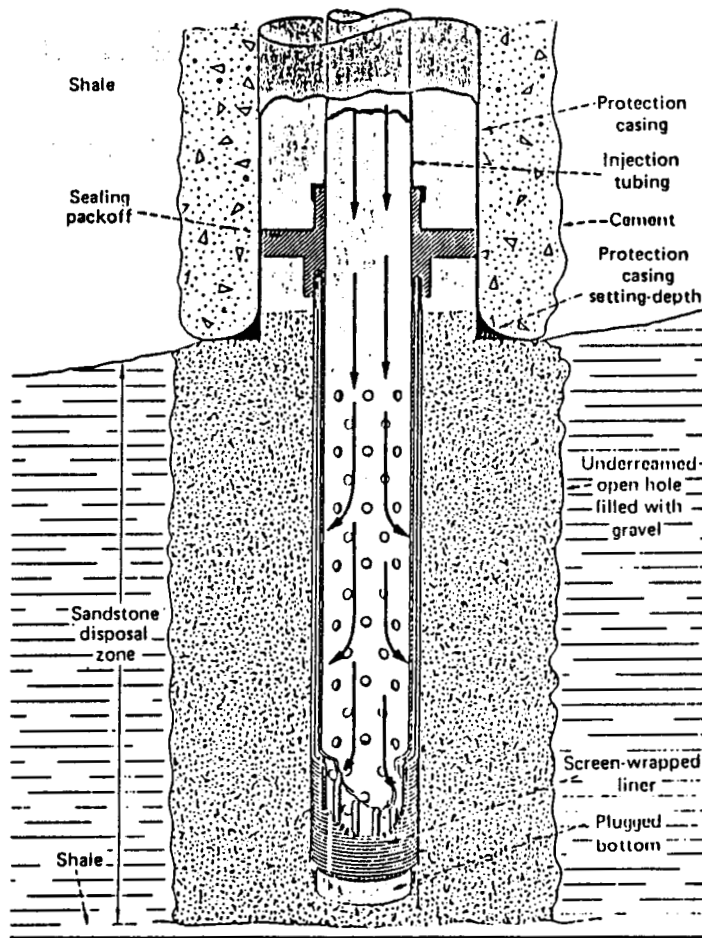


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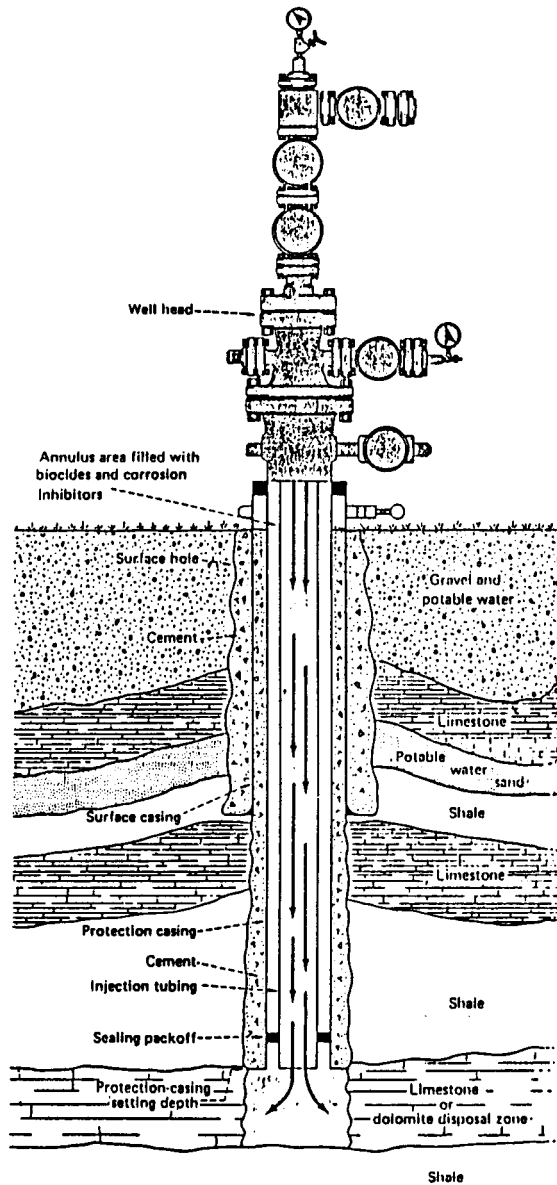
Completion for disposal into
sandstone formation

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Well casing and completion for deepwell
disposal into limestone or dolomite

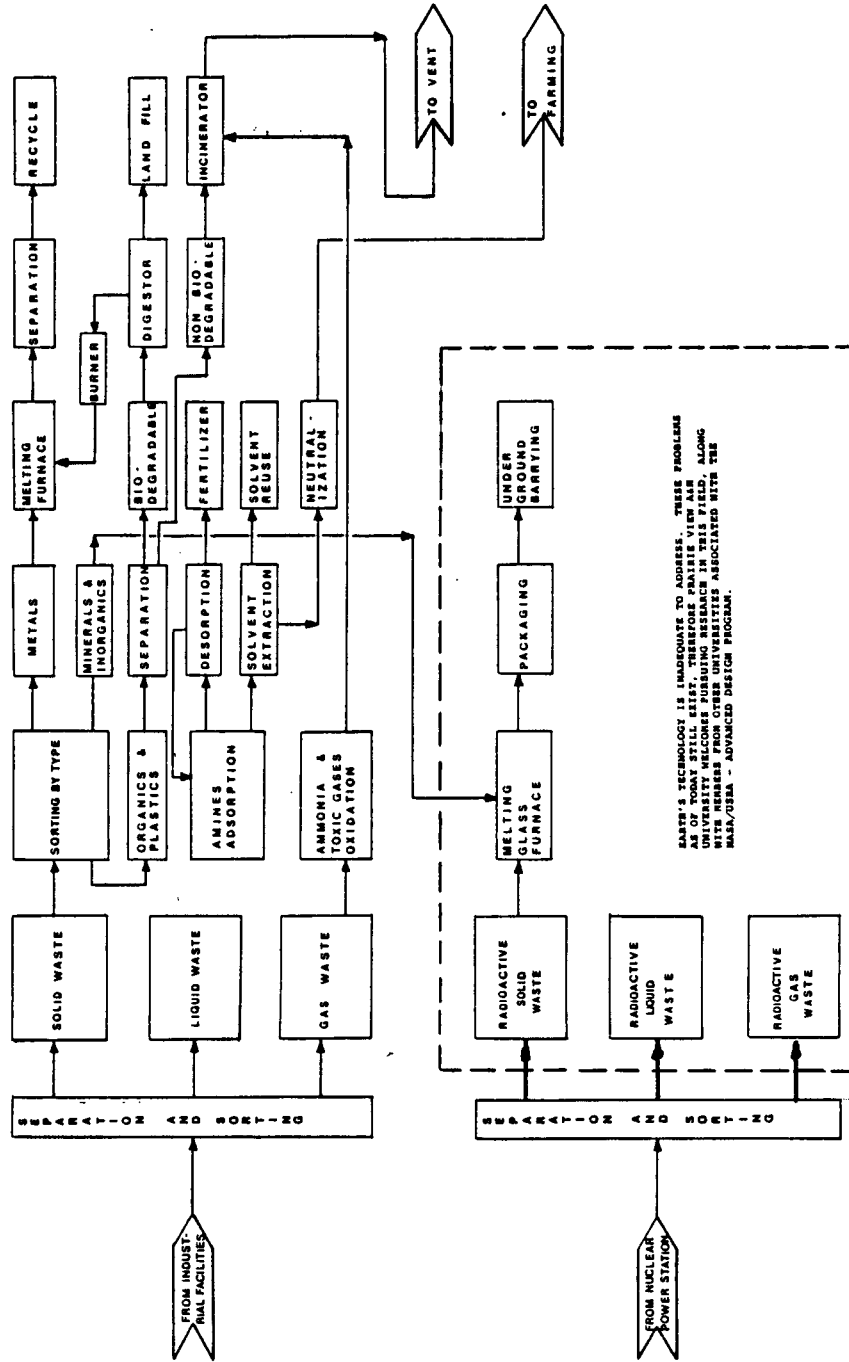
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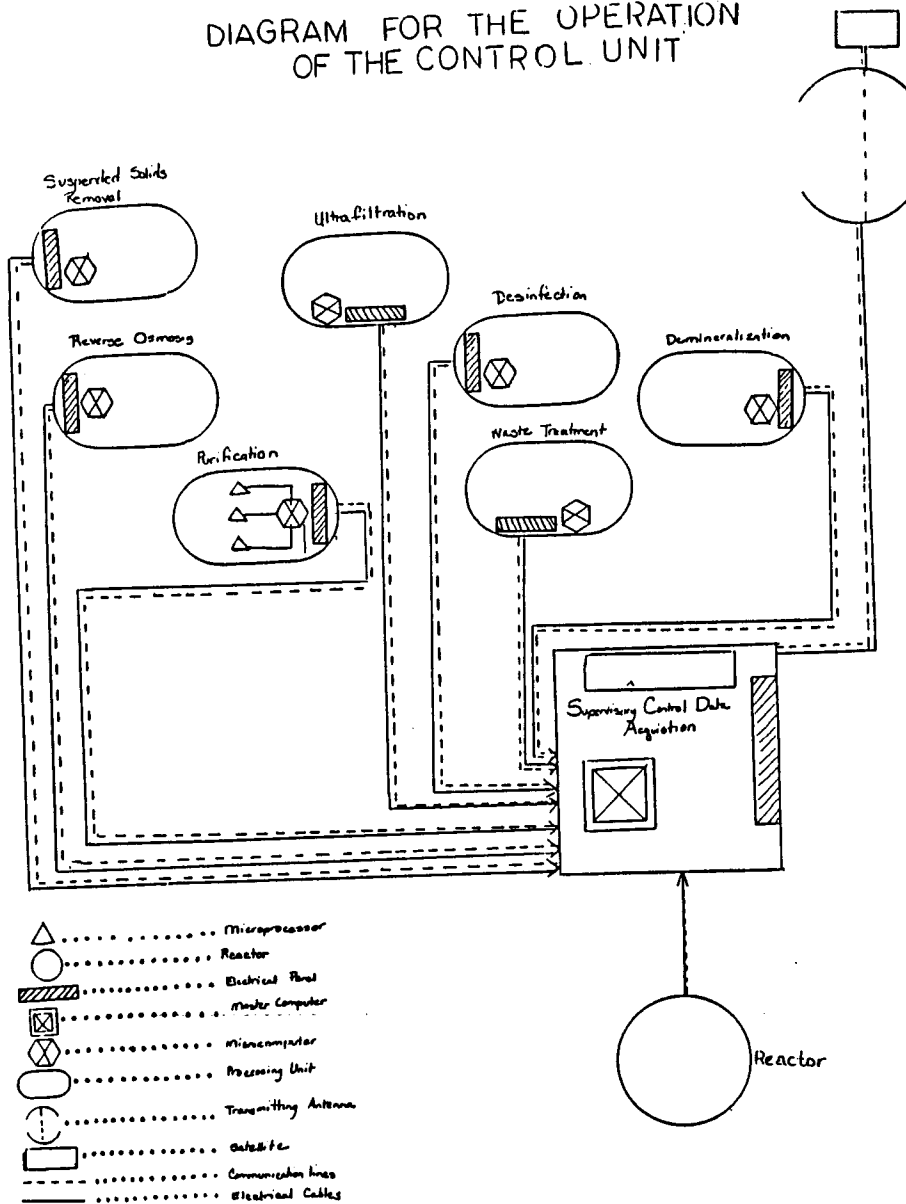
8 HYPOTHETICAL INDUSTRIAL WASTE MANAGEMENT SCHEME



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	NAME K. FOTOUH	DESIGNED BY K. FOTOUH	DATE 1978	PROJECT ADVANCED DESIGN PROJECT
	PROJECT NUMBER 1-B			

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DIAGRAM FOR THE OPERATION
OF THE CONTROL UNIT



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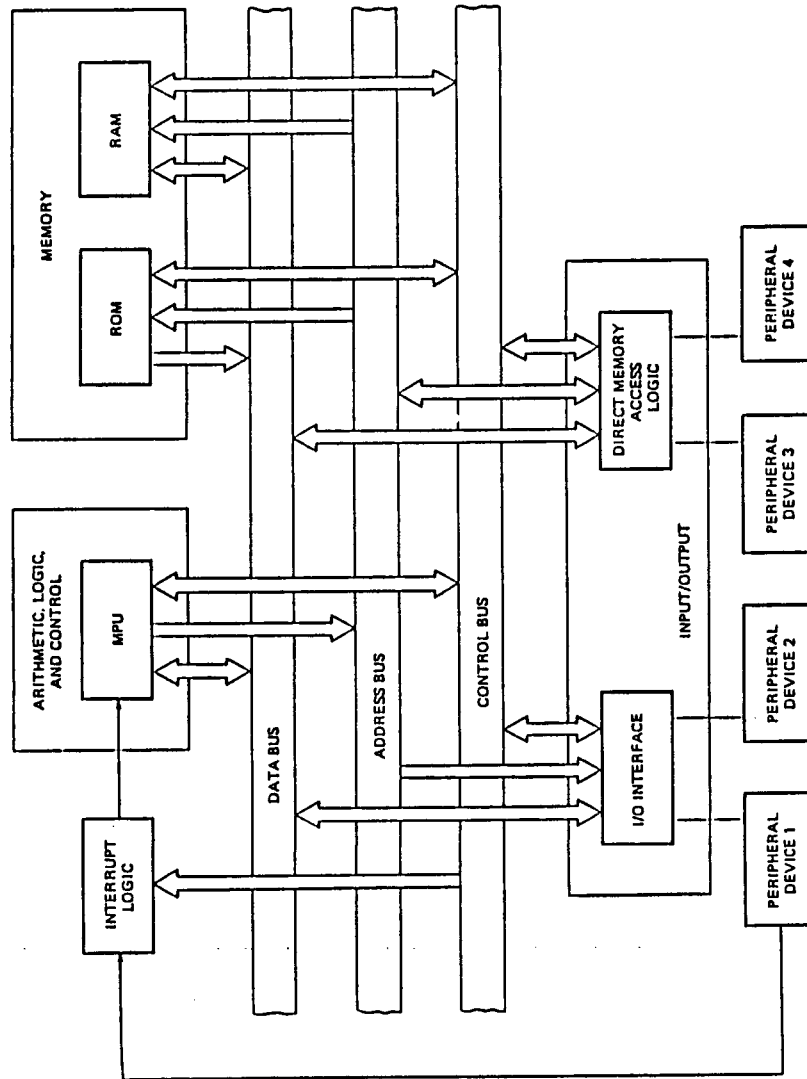


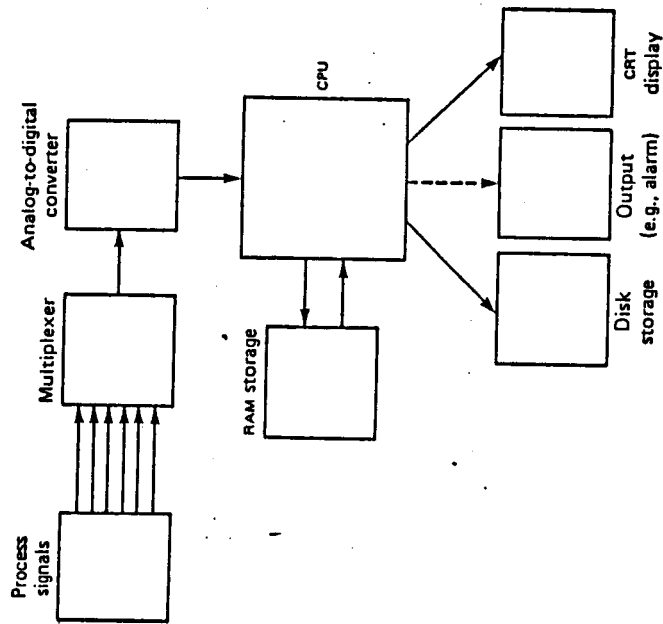
Figure 1 Architecture of a Typical Microcomputer.



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How data move through
the monitoring system



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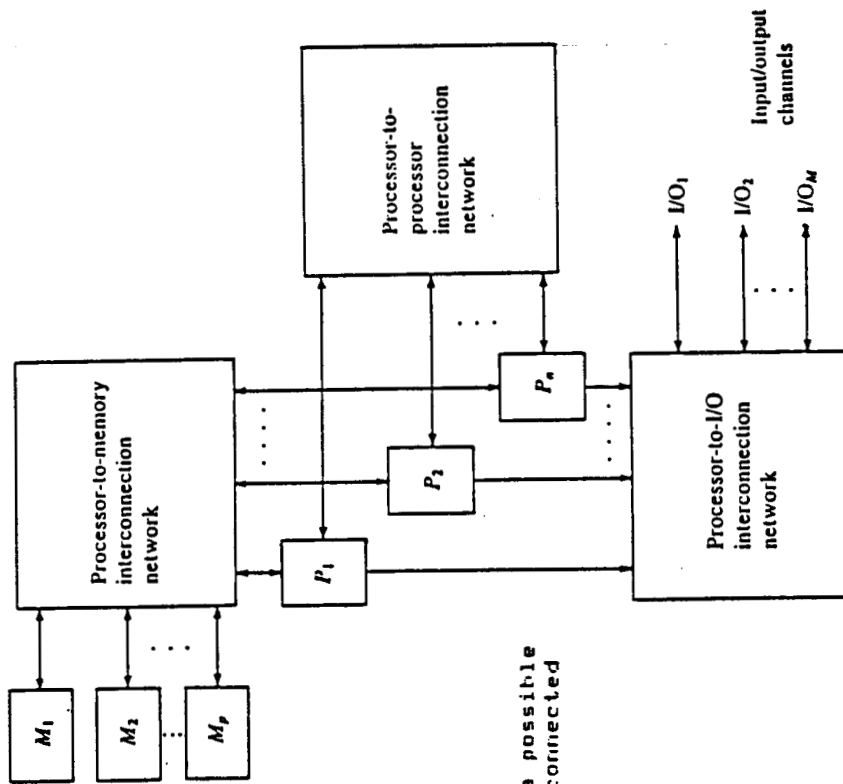
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A simple diagram basically showing a possible way to have several microprocessor connected in our processing units.

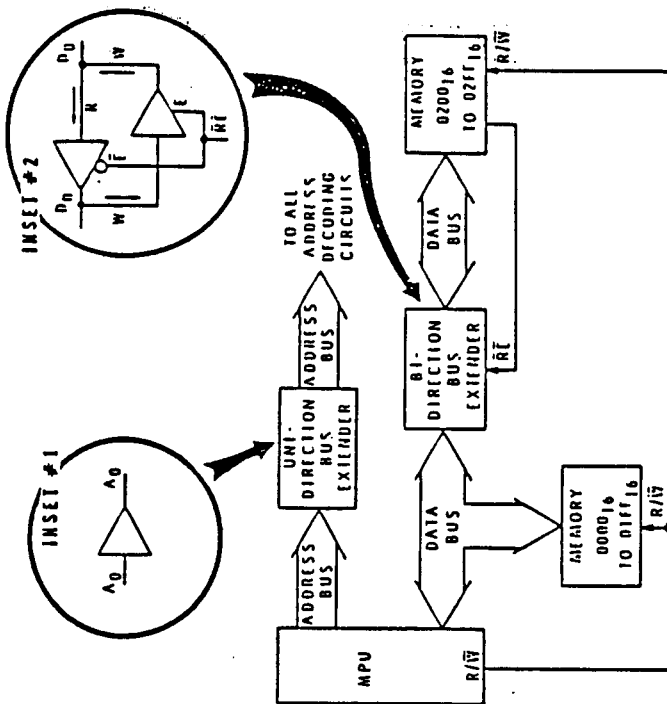


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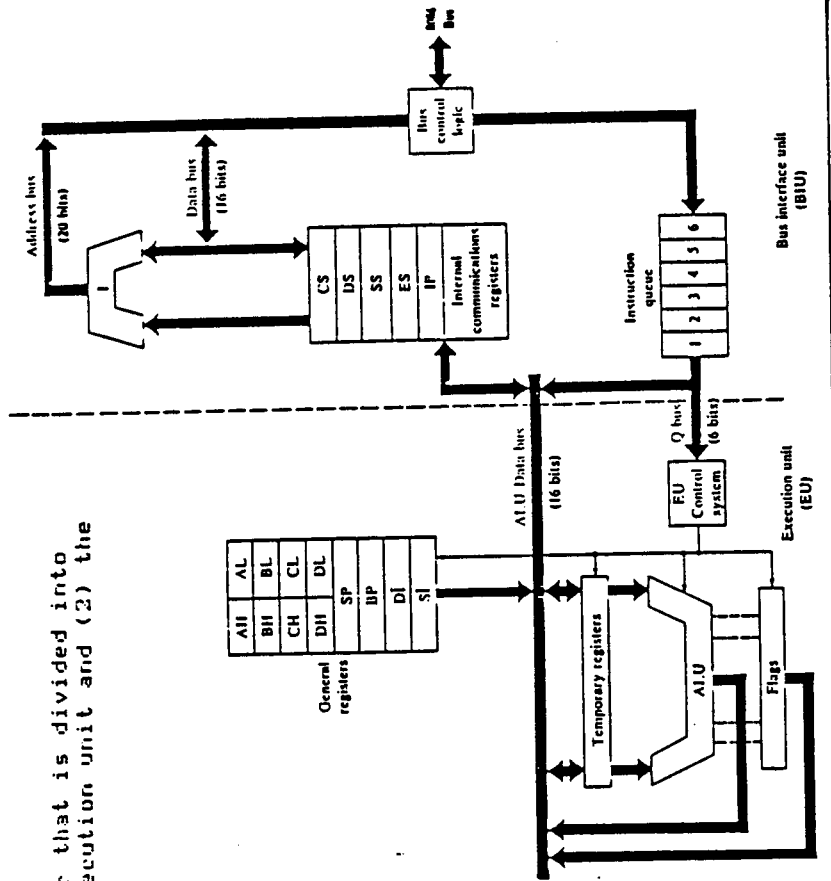
Block diagram of typical microprocessor system using bus extenders.

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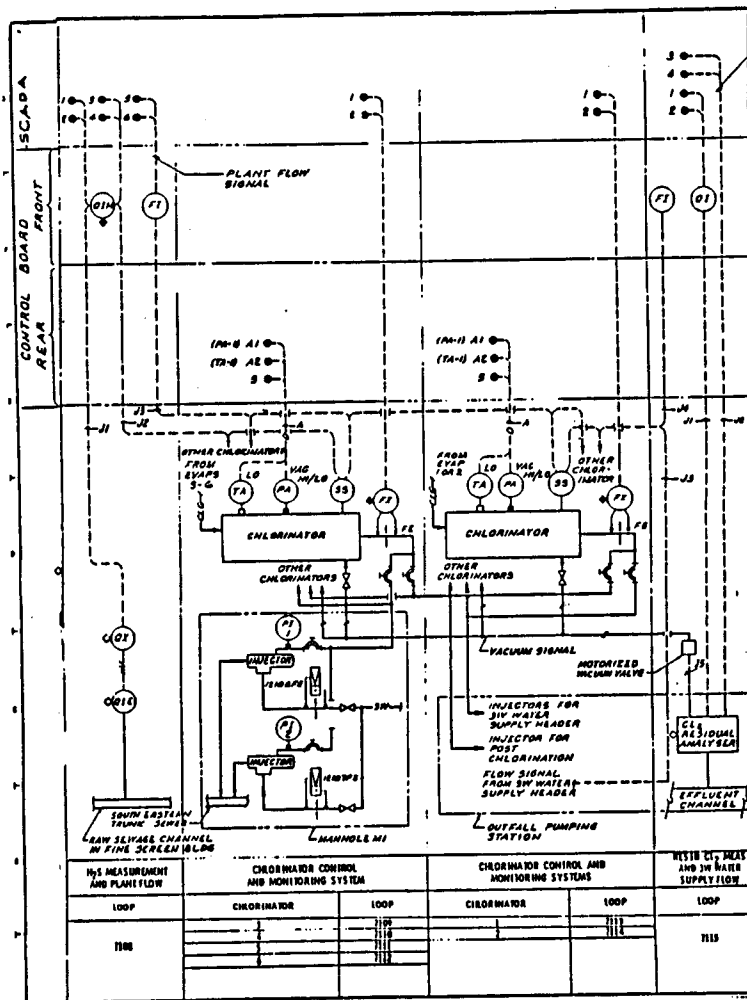
A 16-bit microprocessor that is divided into two parts: (1) the execution unit and (2) the bus interface unit.



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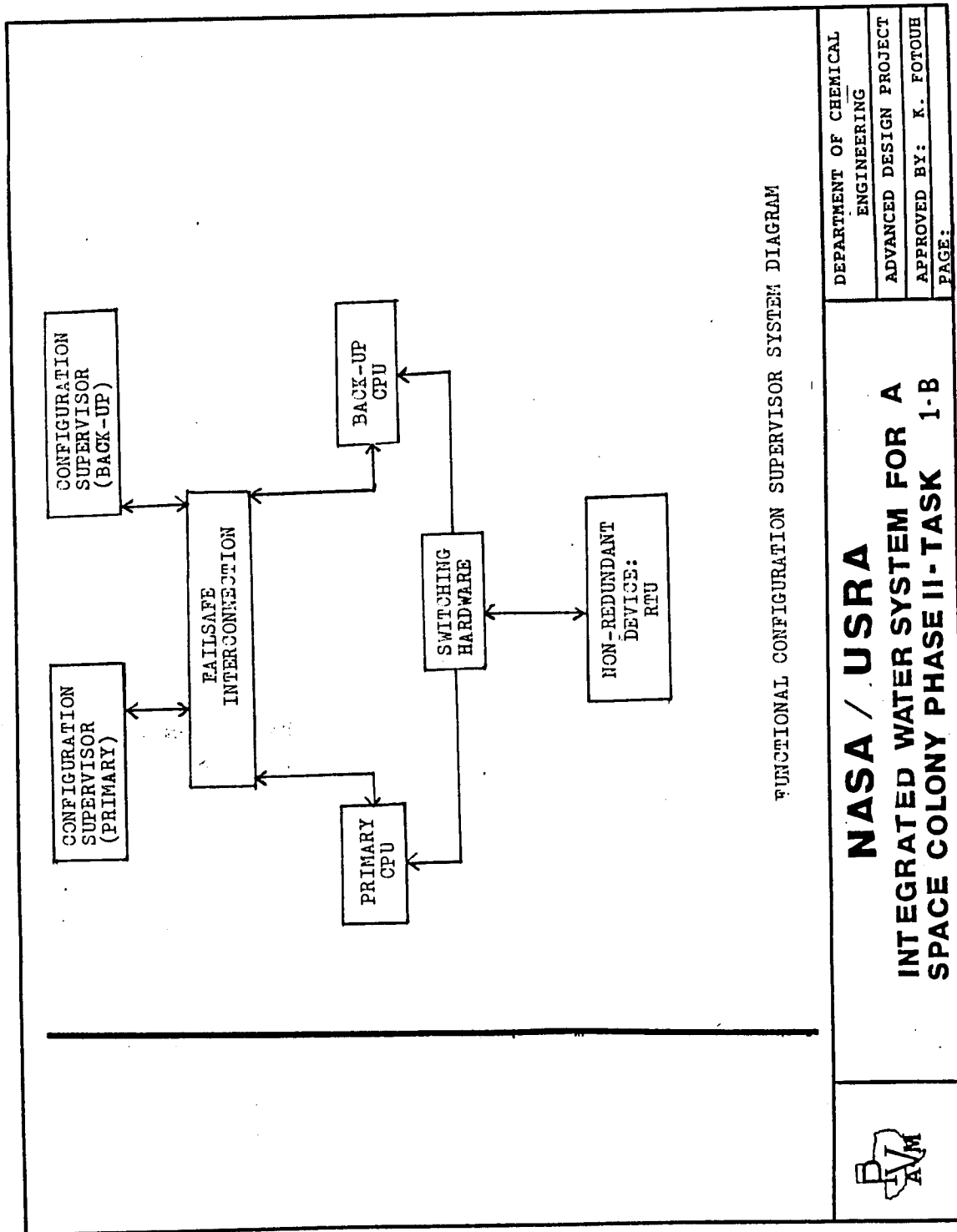


Example of a typical processing plant with alarms controlled by the SCADA.


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SPACE COLONY PHASE II-TASK 1-B

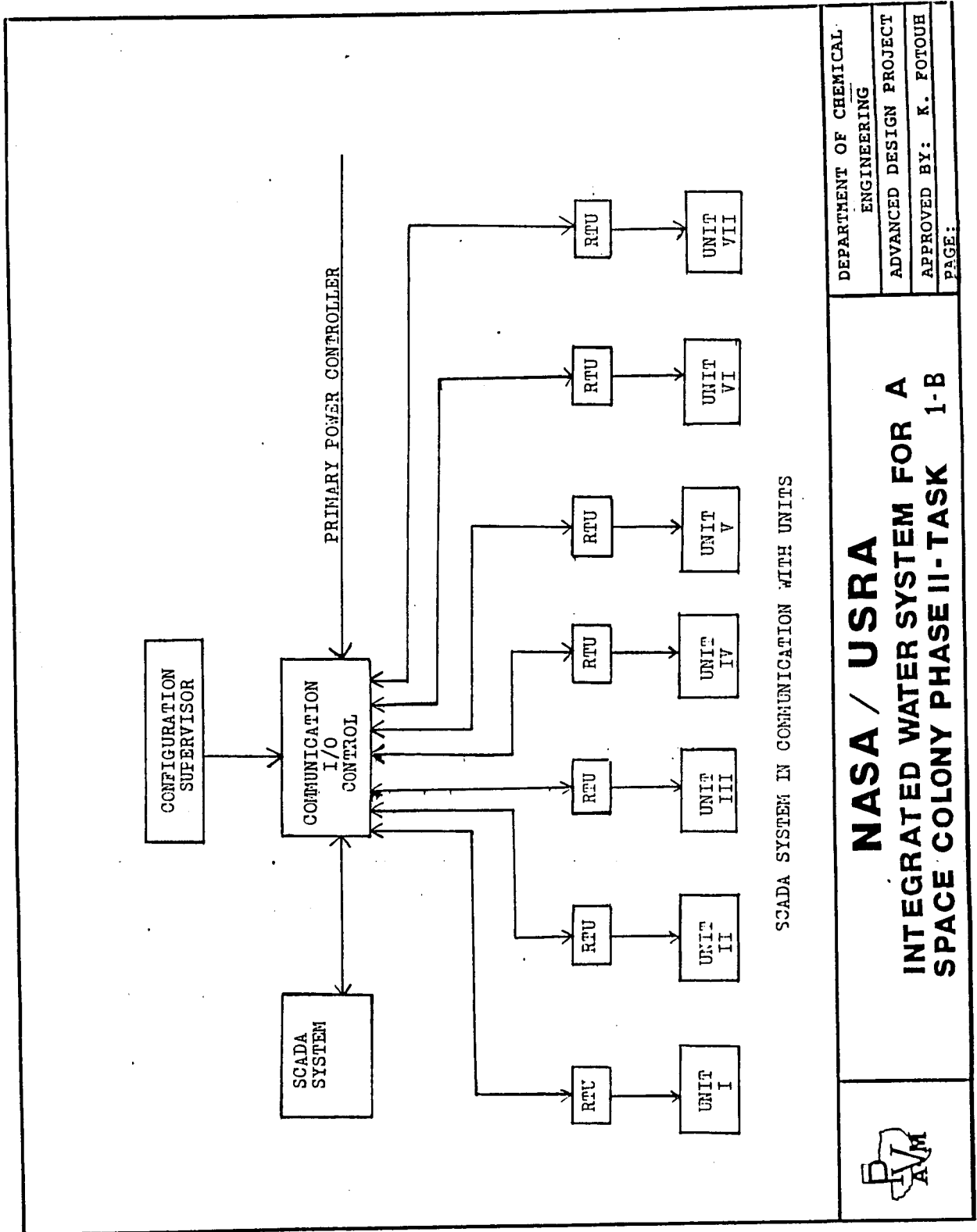




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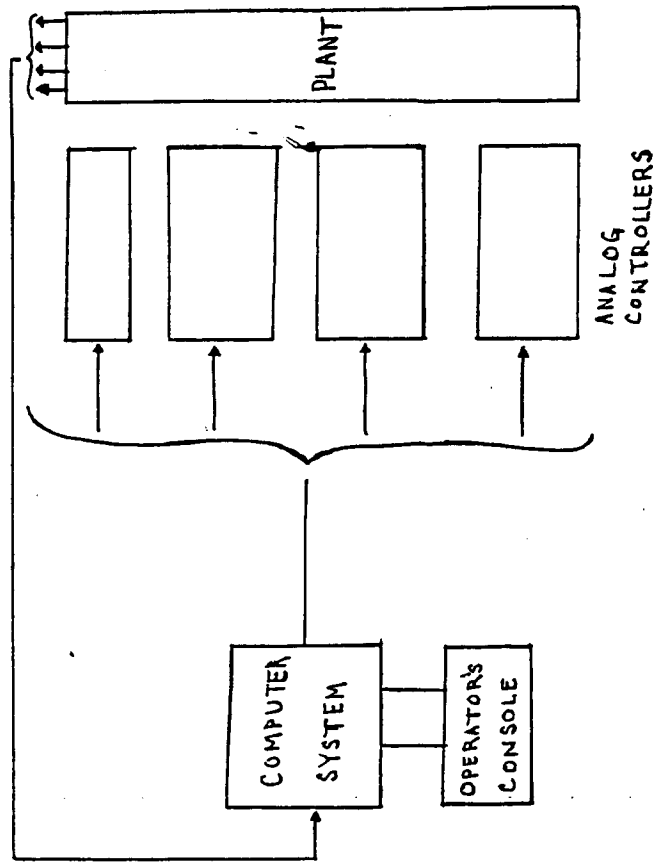
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Supervisory Control System



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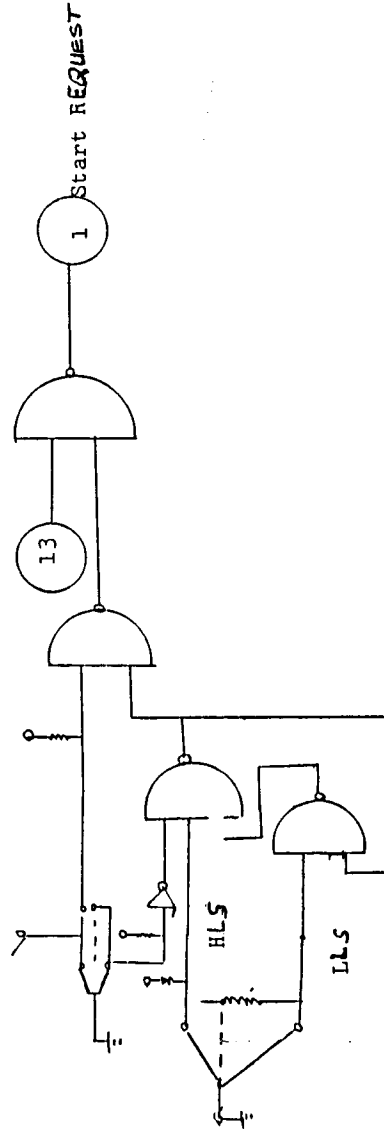
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START REQUEST LOGIC CIRCUIT

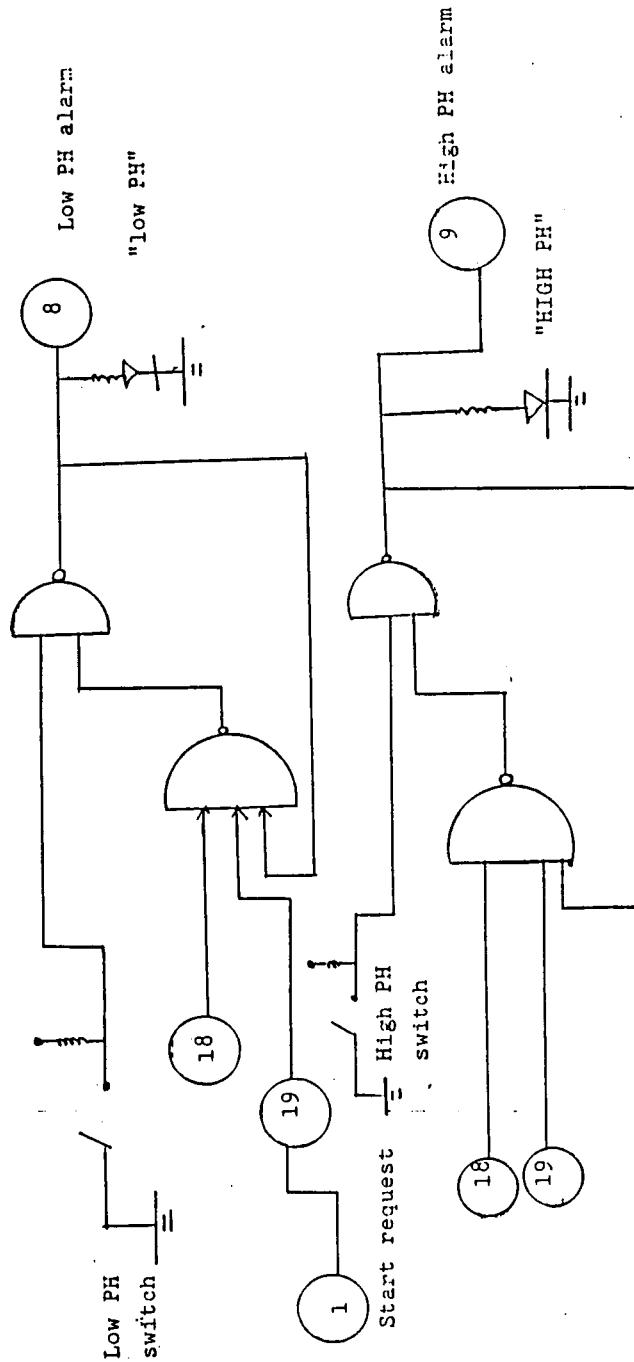


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PH ALARMS USING LOGIC CIRCUIT

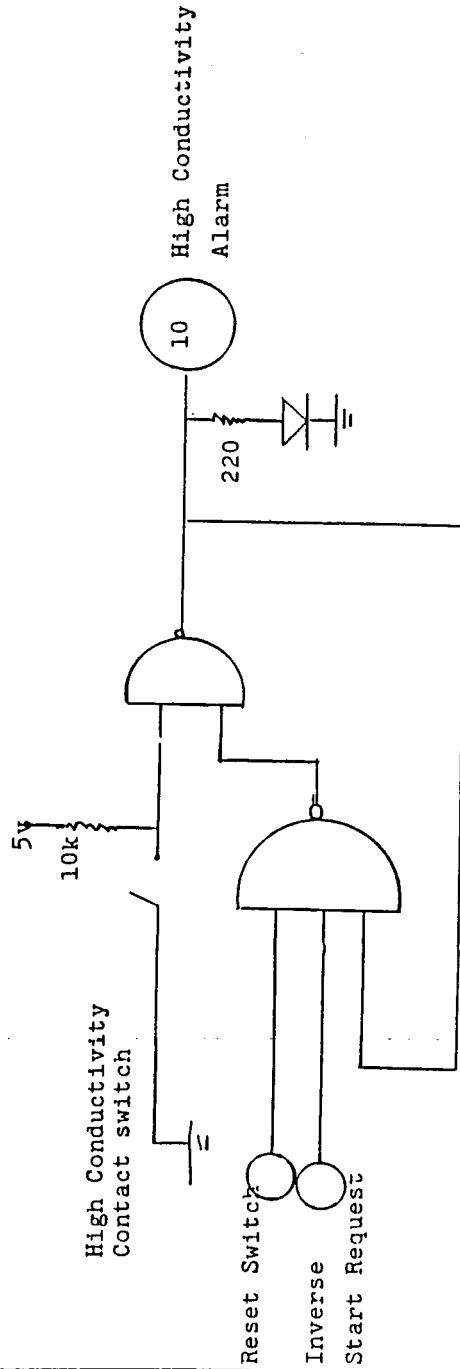


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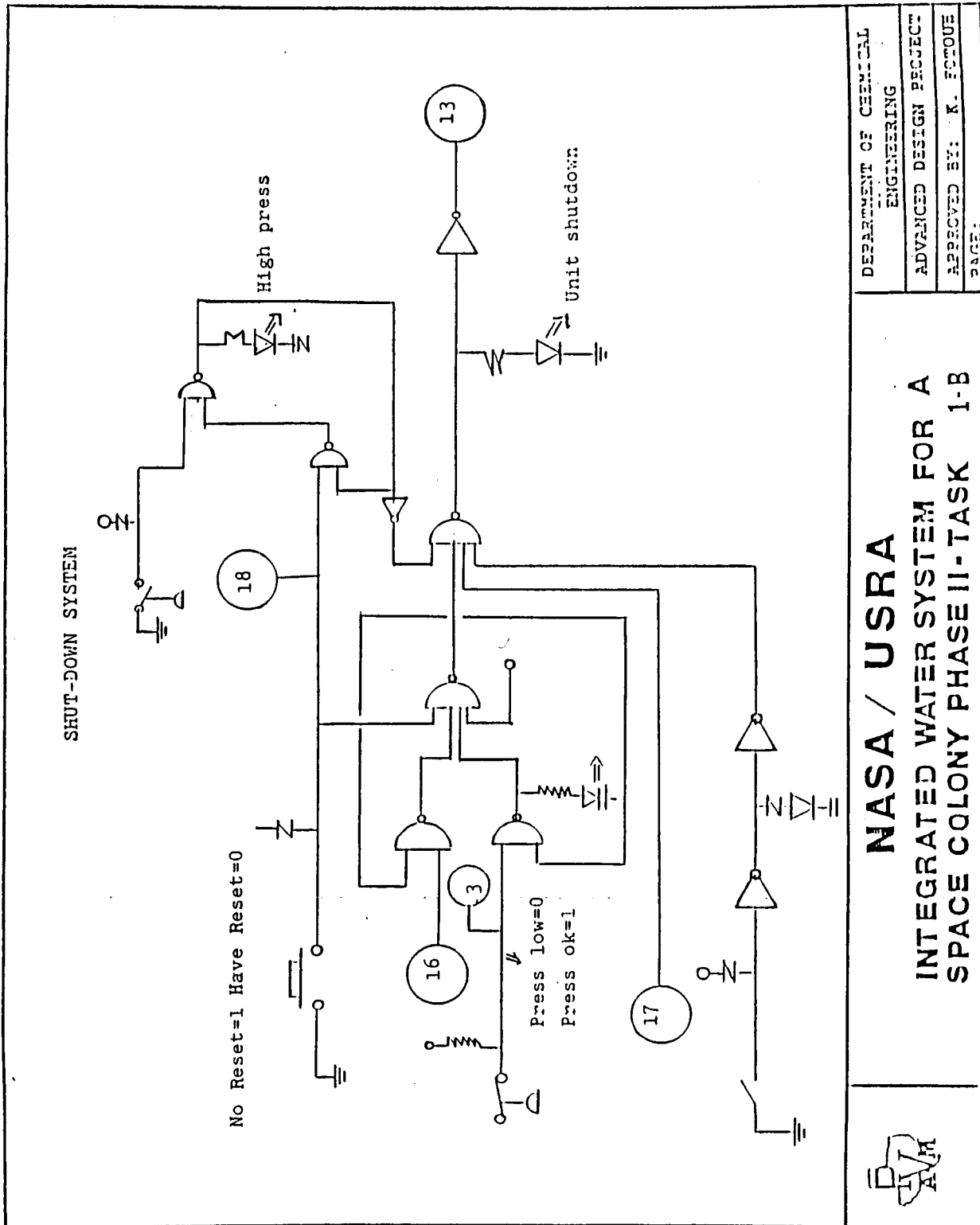
CONDUCTIVITY & MOTOR OVERLOAD ALARMS VS LOGIC CIRCUITS



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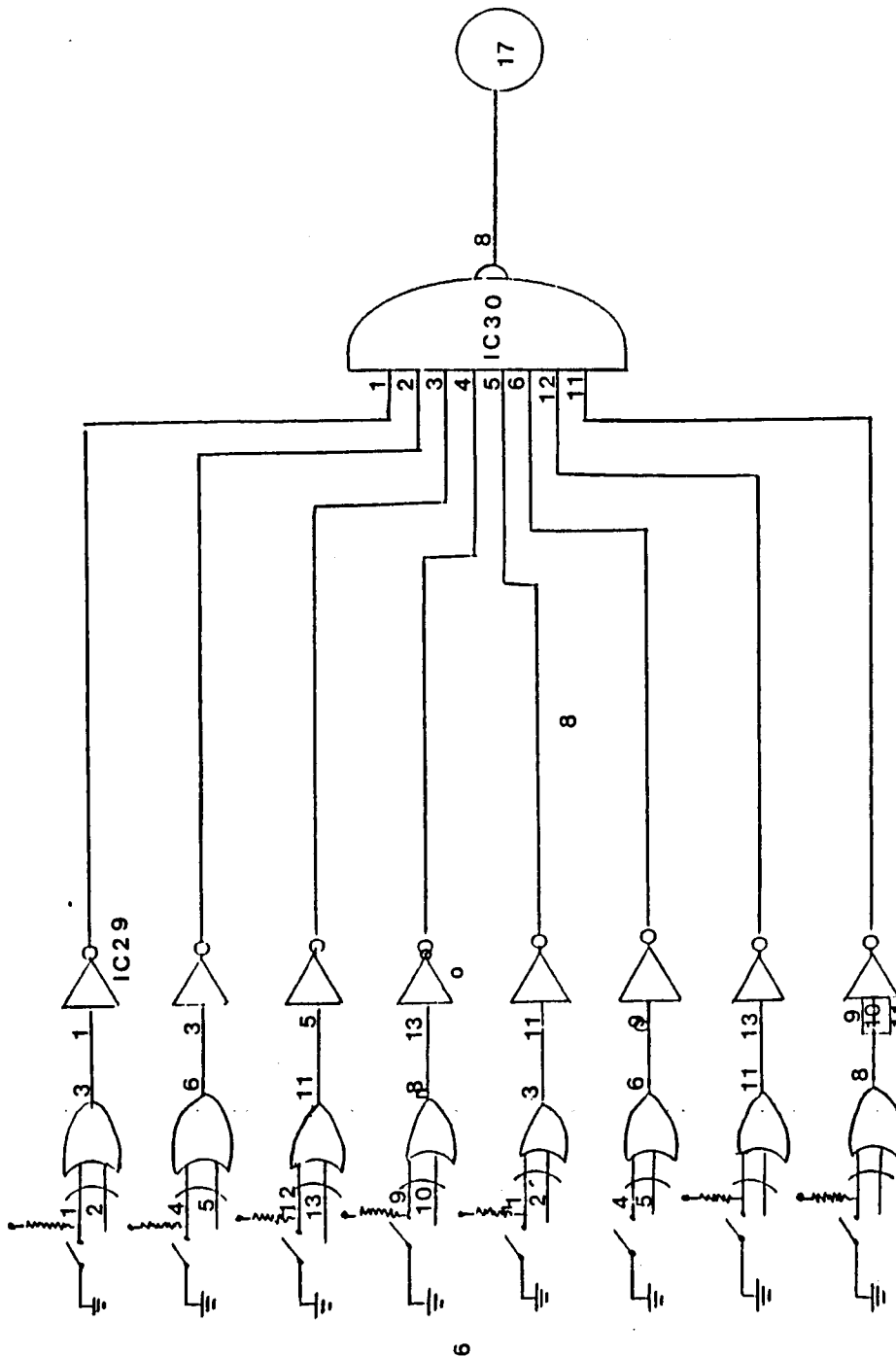
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SET POINT COMPARING CIRCUIT



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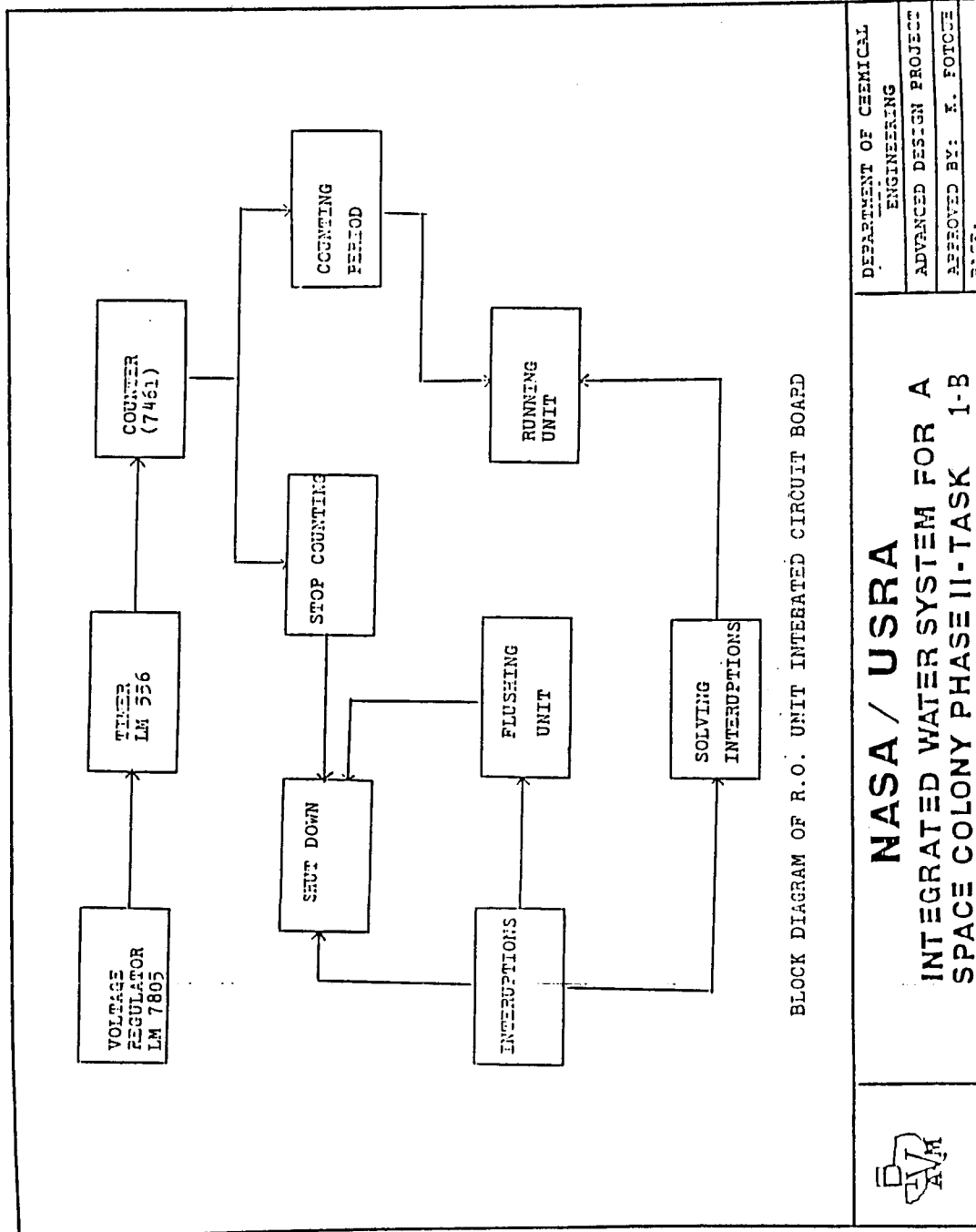
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